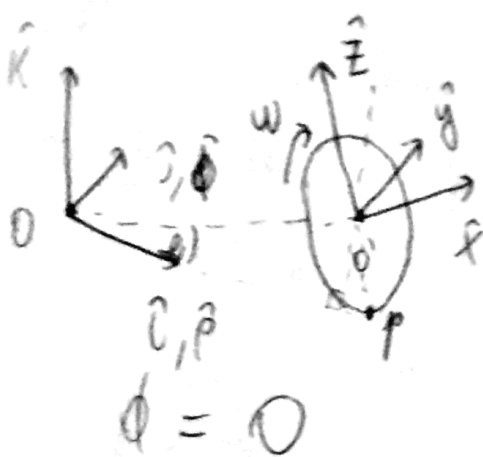


[2]



- O' rote de forma No-SOLIDARIA com a munda, pmo o tel. de $\vec{R}_{cm} = \vec{R}_{O'}$, y $\hat{x}, \hat{z}, \hat{y}$ ston en los etes principales $\rightarrow$ rote con velocidade $\Omega \hat{K}$

$$\begin{aligned} \vec{R}_{O'} &= \rho \hat{\rho} + z \hat{K} = \cancel{b \hat{\rho}} + \cancel{b \hat{K}} \\ &= (b - e \sin \theta) \hat{\rho} + e \cos \theta \hat{K} \\ \Rightarrow \vec{V}_{O'} &= (b - e \sin \theta) \dot{\phi} \hat{\phi} \end{aligned}$$

- Condición de rodadura

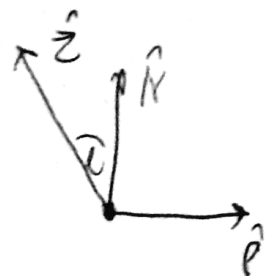
$$\rightarrow \vec{V}_p = \vec{V}_{cm} + \vec{\omega}_{cuerpo} \times \vec{r}_{cm \rightarrow p} = 0$$

- $\vec{\omega}_{cuerpo}$ es la suma de $\vec{\omega}$ y $\vec{\Omega}$ (rotación + precesión)

$$\rightarrow (b - e \sin \theta) \dot{\phi} \hat{\phi} + (\vec{\omega} + \vec{\Omega}) \times (-e \hat{z}) = 0$$

$$\rightarrow (b - e \sin \theta) \dot{\phi} \hat{\phi} + (-\omega \hat{x} + \Omega \hat{K}) \times (-e \hat{z}) = 0$$

$$\begin{aligned} \hat{x} \times \hat{z} &= -\hat{y} = -\hat{\phi}, \quad \hat{K} \times \hat{z} = \hat{K} \times (\hat{K} \cos \theta - \hat{\rho} \sin \theta) \\ &= \cancel{\cos \theta} - \sin \theta \hat{\phi} \end{aligned}$$



$$\rightarrow (b - a \sin \ell) \dot{\phi} \hat{\phi} + a(-\omega \hat{\phi} + \Omega \sin \ell \hat{\phi}) = 0$$

$$\rightarrow b\Omega - a\omega = 0 \rightarrow \omega = \frac{b\Omega}{a} \quad \text{lo guardamos}$$

• busamos $\vec{L}_{cm}$, para usar las ecuaciones de euler

$$\begin{aligned} \vec{L}_{cm} &= I_{cm} \vec{\omega}_{cuerpo} \quad (\text{en base de } O', \text{ tenemos la sft}) \\ &= I_{cm} (-\omega \hat{x} + \Omega \hat{k}) = I_{cm} (-\omega \hat{x} + \Omega (\sin \ell \hat{x} + \cos \ell \hat{z})) \\ &= I_{cm}^{11} (a \sin \ell - \omega) \hat{x} + I_{cm}^{33} \Omega \cos \ell \hat{z} \end{aligned}$$



$$I_{cm}^{11} = \int_V (\|\vec{r}\|^2 \delta_{11} - r_1 r_1) dV = \int_V \|\vec{r}\|^2 dV$$

Usamos cilíndricos

$$dV = \frac{m}{\pi a^2} \rho d\phi d\rho, \quad \|\vec{r}\| = \rho, \quad \phi \in [0, 2\pi], \quad \rho \in [0, a]$$

$$\rightarrow I_{cm}^{11} = \int_0^a \int_0^{2\pi} \rho^2 \cdot \frac{m}{\pi a^2} \rho d\phi d\rho = \frac{ma^2}{2}$$

$$I_{cm}^{33} = \int_V (\|\vec{r}\|^2 \delta_{33} - r_3 r_3) dV, \quad \vec{r} = \rho \hat{\rho} = \rho (\cos \psi \hat{y} + \sin \psi \hat{z})$$

$$\rightarrow r_{33} = \rho \sin \psi \hat{z}$$

$$= \int_0^a \int_0^{2\pi} \left(\frac{\rho^2 - \rho^2 \sin^2 \psi}{\rho^2 \cos^2 \psi} \right) \frac{m}{\pi a^2} \rho d\psi d\rho = \frac{ma^2}{4}$$

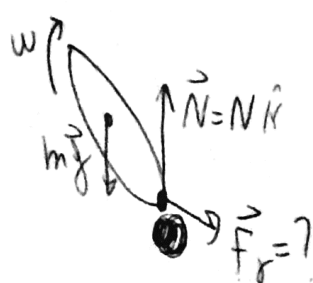
$$\vec{L}_{cm} = m e^2 \left(\frac{(\omega \sin \theta - \dot{\phi}) \hat{x}}{2} + \frac{\Omega \cos \theta \hat{z}}{4} \right) \quad \text{constante para 0'}$$

• ahora calculamos el torque neto con respecto al cm

DCL

$$m \ddot{\vec{R}}_{cm} = \left((b - e \sin \theta) \dot{\phi}^2 \right) \hat{\rho} = \vec{N} + m \vec{g} + \vec{F}_r$$

$\Omega = \dot{\phi}$



$$\rightarrow -(b - e \sin \theta) \dot{\phi}^2 \hat{\rho} = N \hat{R} - m g \hat{r} + \vec{F}_r$$

$$\rightarrow N = m g$$

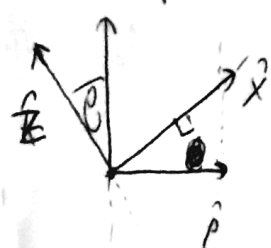
$$\vec{F}_r = -\frac{1}{2}(b - e \sin \theta) \dot{\phi}^2 \hat{\rho} \quad (F_r \text{ ha que ser compoente vertical})$$

$$\rightarrow \vec{\tau}_{\vec{N}} = (-e \hat{z}) \times (m g \hat{r})$$

$$= -m g e (\hat{z} \times (\sin \theta \hat{x} + \cos \theta \hat{z}))$$

$$= -m g e \sin \theta \hat{y}$$

$$\vec{\tau}_{\vec{F}_r} = (-e \hat{z}) \times \left(\frac{1}{2}(b - e \sin \theta) \dot{\phi}^2 \hat{\rho} \right)$$



$$= m e (b - e \sin \theta) \dot{\phi}^2 \hat{z} \times (\hat{x} \sin \theta - \hat{z} \cos \theta)$$

$$= -m e (b - e \sin \theta) \dot{\phi}^2 \sin \theta \hat{y}$$

• ec. de Euler

$$\rightarrow \underbrace{\left(\frac{d\vec{L}_{cm}}{dt} \right)}_{\text{SRNI}} + \vec{\omega}_{sys} \times \vec{L}_{cm} = \vec{\tau}_{cm}$$

$$0 + (\Omega (\sin \theta \hat{x} + \cos \theta \hat{z})) \times \frac{m e^2}{2} ((\Omega \sin \theta - \dot{\phi}) \hat{x} + \frac{\Omega \cos \theta}{2} \hat{z})$$

$$= -m e \hat{y} (g \sin \theta + \Omega^2 (b - e \sin \theta) \cos \theta)$$

$$\rightarrow \frac{1}{2} \frac{e^4}{\hbar^2} \Omega \left(\frac{e \cos \theta \sin \ell}{2} (-\dot{y}) + (\Omega \sin \ell - \omega) \cos \ell \dot{y} \right)$$

$$= - \frac{1}{2} \frac{e^4}{\hbar^2} \dot{y} \left(y \sin \ell + \Omega^2 (b - e \sin \ell) \cos \ell \right)$$

$$\rightarrow \frac{e \Omega}{2} \left(\cos \ell (\Omega \sin \ell - \omega) - \Omega \frac{\cos \ell \sin \ell}{2} \right)$$

$$= - \left(y \sin \ell + \Omega^2 (b - e \sin \ell) \cos \ell \right)$$

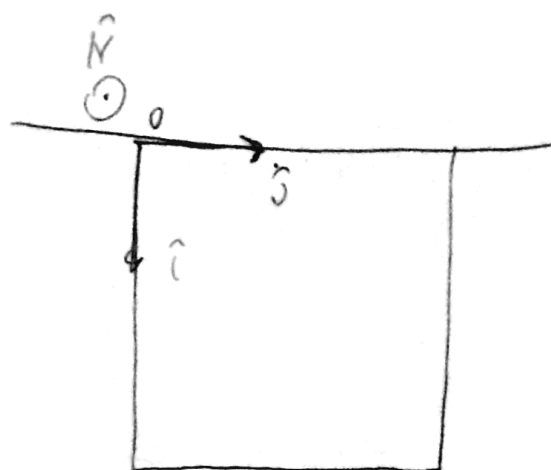
$$\Rightarrow \Omega^2 = \frac{y \sin \ell}{6b \cos \ell - 5e \sin \ell \cos \ell}$$

$$\omega = \frac{b \Omega}{e}$$

Note that for $6b \cos \ell - 5e \sin \ell \cos \ell > 0$

$$\rightarrow 6b > 5e \sin \ell$$

$$\rightarrow b > \frac{5e}{6} \sin \ell //$$



$$\vec{\omega} = \dot{\theta} \hat{j}$$

• $\hat{j}$ No es un eje principal, necesito cada

$$I_0$$

$$I_{ij} = \int_V (\|\vec{r}\|^2 \delta_{ij} - r_i r_j) dm$$

• Usar coordenadas

$$I_0 = \int_V \begin{bmatrix} y^2 & -xy & 0 \\ -xy & x^2 & 0 \\ 0 & 0 & x^2 + y^2 \end{bmatrix} \frac{M}{a^2} dx dy$$

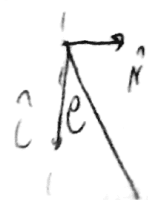
$$= \int_0^a \int_0^a \frac{M}{a^2} \begin{bmatrix} y^2 dx dy & -xy dx dy & 0 \\ -xy dx dy & x^2 dx dy & 0 \\ 0 & 0 & (x^2 + y^2) dx dy \end{bmatrix}$$

$$= M a^2 \begin{bmatrix} 1/3 & -1/4 & 0 \\ -1/4 & 1/3 & 0 \\ 0 & 0 & 2/3 \end{bmatrix}$$

$$\vec{L}_0 = I_0 \vec{\omega} = \begin{bmatrix} 1/3 & -1/4 & 0 \\ -1/4 & 1/3 & 0 \\ 0 & 0 & 2/3 \end{bmatrix} \begin{bmatrix} 0 \\ \dot{\theta} \\ 0 \end{bmatrix} M a^2 = M a^2 \begin{bmatrix} -\dot{\theta}/4 \\ \dot{\theta}/3 \\ 0 \end{bmatrix}$$

$$\text{entonces } K = \frac{\vec{\omega} \cdot \vec{L}_0}{2} = \frac{M a^2}{2} \begin{bmatrix} 0 \\ \dot{\theta} \\ 0 \end{bmatrix} \cdot \begin{bmatrix} -\dot{\theta}/4 \\ \dot{\theta}/3 \\ 0 \end{bmatrix} = \frac{M a^2 \dot{\theta}^2}{6}$$

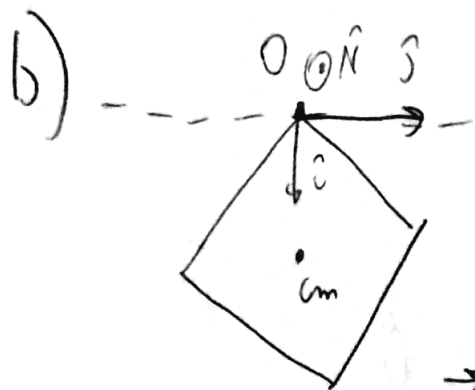
y además $U = -M g \frac{a}{2} \cos \theta$



$$\hookrightarrow \mathcal{L} = \frac{M a^2 \dot{\theta}^2}{6} + \frac{M g a \cos \theta}{2}$$

$$\frac{d}{dt} \left(\frac{\partial \mathcal{L}}{\partial \dot{\theta}} \right) - \frac{\partial \mathcal{L}}{\partial \theta} = 0 \rightarrow \frac{M e^2}{3} \ddot{\theta} + \frac{m g e}{2} \sin \theta = 0$$

$$\rightarrow \ddot{\theta} = -\frac{3g}{2e} \sin \theta$$



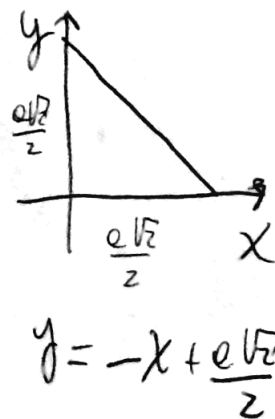
• En este caso, $\hat{S}$ sí es un eje principal

$$\rightarrow I_0 \vec{\omega} = I_{22}^0 \dot{\theta} \hat{S}$$

Por Steiner, $I_{22}^0 = I_{22}^{cm} + M \left(\frac{e\sqrt{2}}{2} \right)^2$

• Como I es aditivo, podemos calcular I para un cuarto, y sumar los (por simetría, todos son iguales)

$$\therefore 4 I_{22}^{cm} = \cancel{I_{22}^0} = \frac{4}{e^2} \int_0^{\frac{e\sqrt{2}}{2}} \int_0^{\frac{e\sqrt{2}}{2}-x} (x^2 + y^2 - x^2) \frac{M}{e^2} dy dx$$



$$= \frac{4M}{e^2} \int_0^{\frac{e\sqrt{2}}{2}} \frac{\left(\frac{e\sqrt{2}}{2} - x \right)^3}{3} dx = \frac{4M e^2}{40} = \frac{M e^2}{12}$$

$$K = \frac{\vec{w} \cdot \left[\left(\frac{M_e^2}{12} + \frac{M_e^2}{2} \right) \vec{w} \right]}{24}$$

$$= \frac{7M_e^2}{24} \dot{\theta}^2$$

$$U = -m g \frac{e\sqrt{z}}{2} \cos \theta$$

$$\rightarrow \mathcal{L} = K - U = \frac{7M_e^2}{24} \dot{\theta}^2 + m g \frac{e\sqrt{z}}{2} \cos \theta$$

$$\frac{d}{dt} \left(\frac{\partial \mathcal{L}}{\partial \dot{\theta}} \right) - \frac{\partial \mathcal{L}}{\partial \theta} = 0 \rightarrow \frac{7M_e^2}{12} \ddot{\theta} + \frac{m g e \sqrt{z}}{2} \sin \theta = 0$$

$$\ddot{\theta} = -\frac{g e \sqrt{z}}{7} \sin \theta$$

$$= -\frac{12}{7\sqrt{2}} \frac{g \sin \theta}{e} //$$