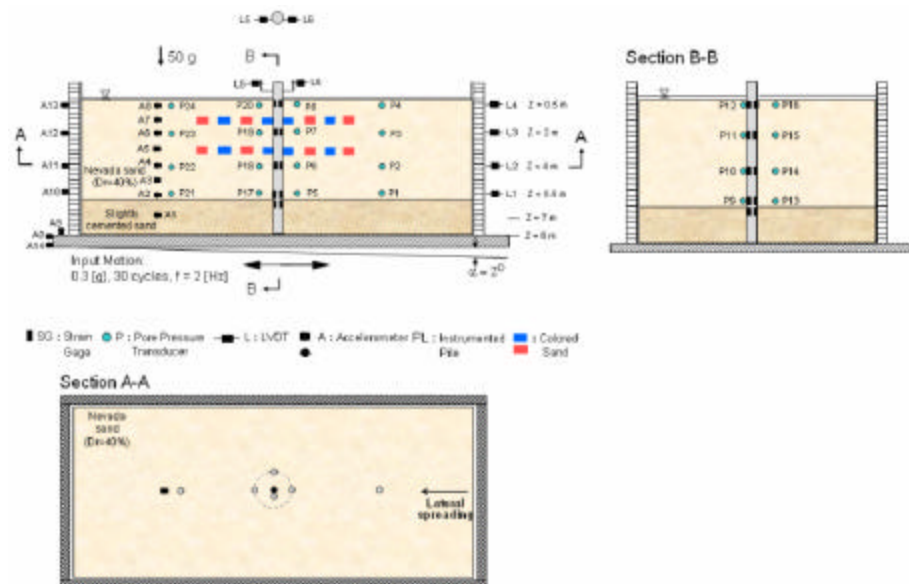


Respuesta de pilotes sometidos a corrimiento lateral de suelo licuado



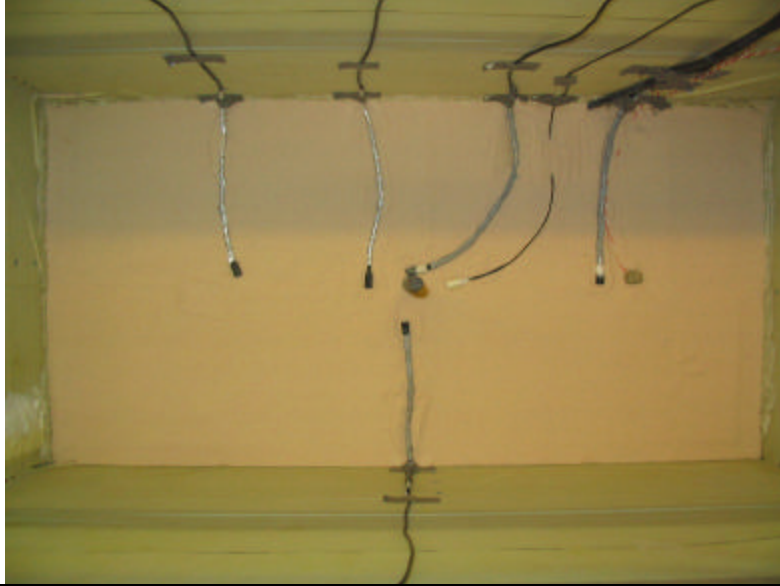
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Esquema de Modelo 1x1-v (saturado con líquido viscoso)



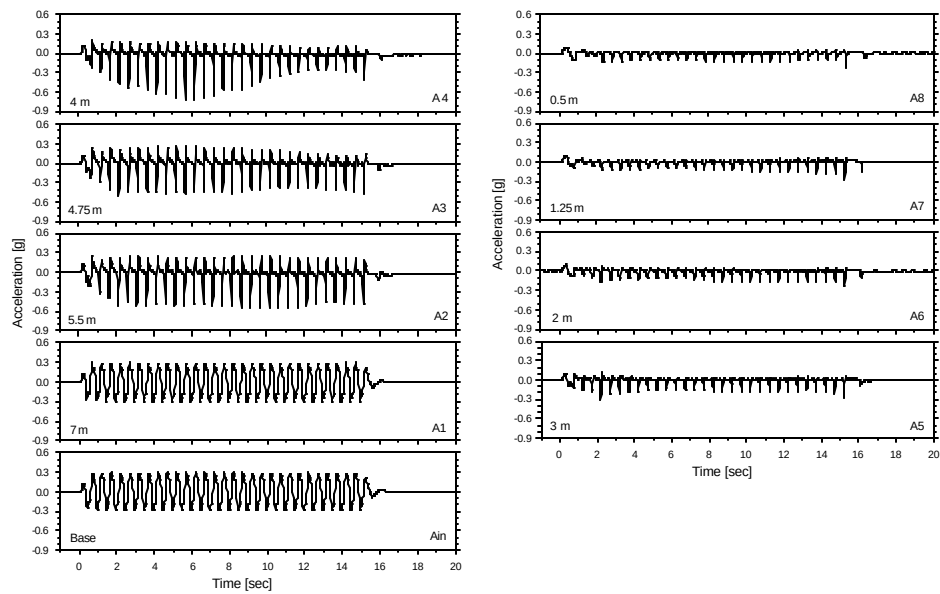
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Preparación del Modelo 1x1-v



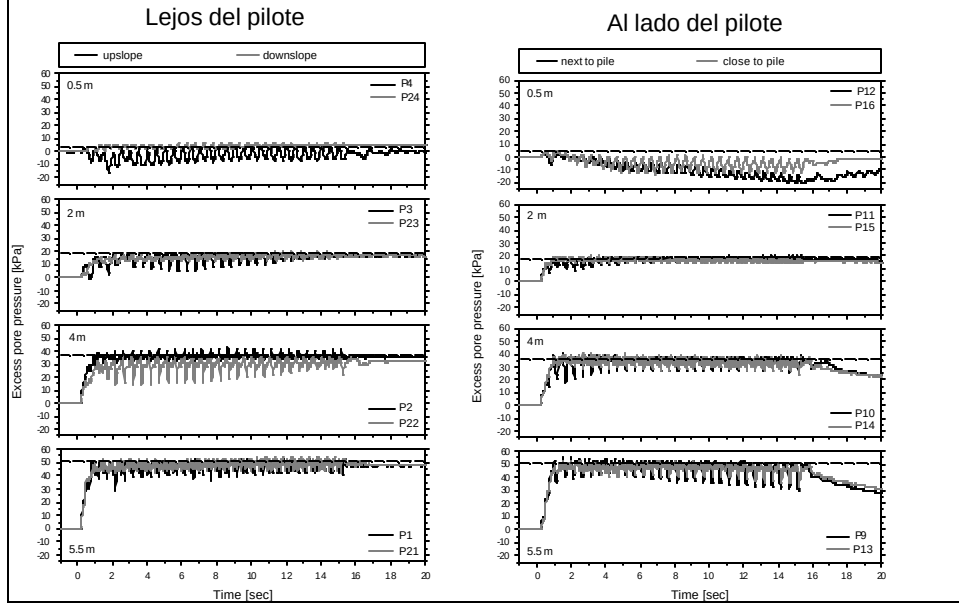
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Historia de aceleraciones



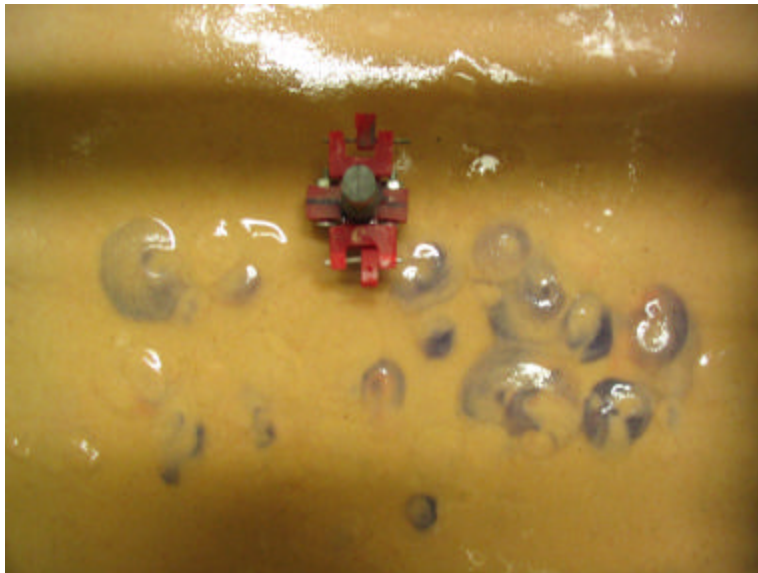
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Exceso de presión de poros



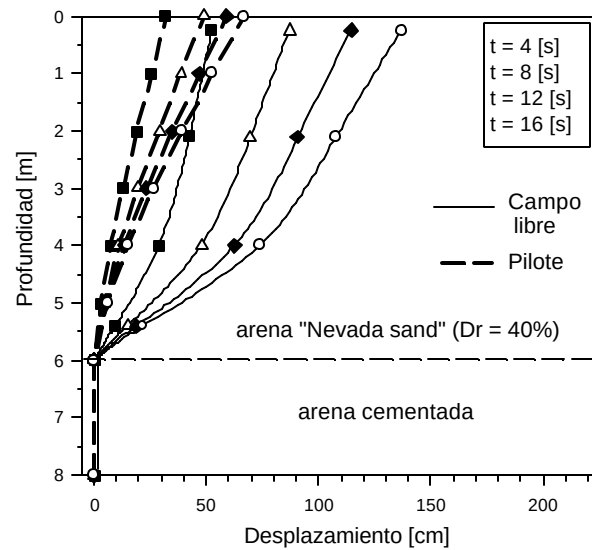
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"Sand boils"



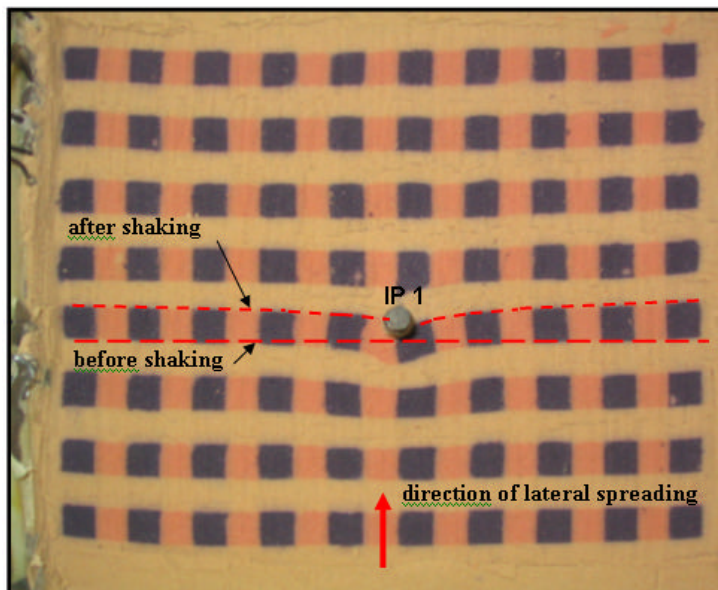
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Perfil de desplazamientos laterales del campo libre y del pilote



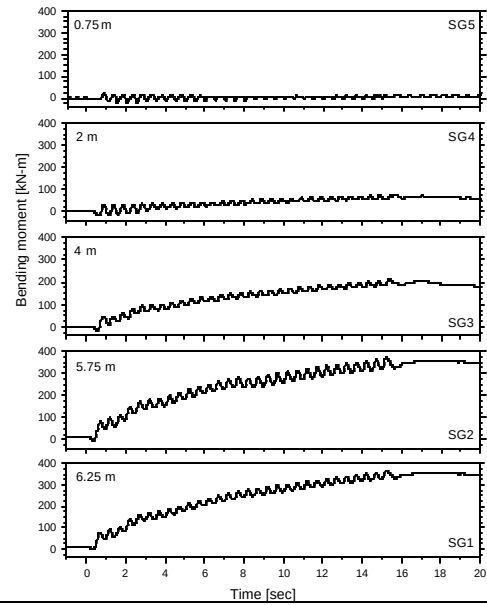
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Patrón de desplazamientos del suelo licuado



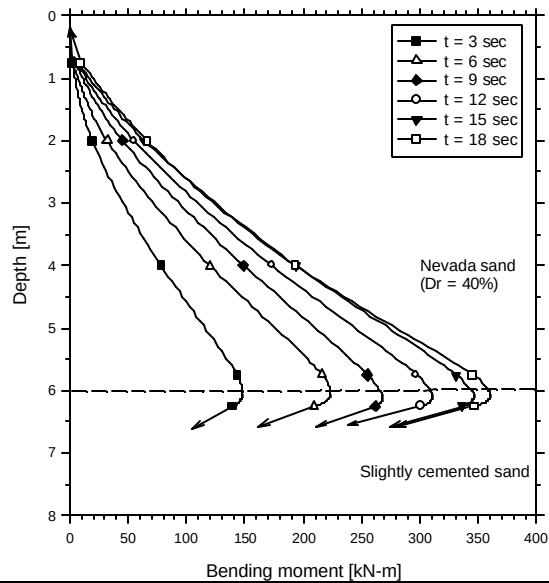
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Historia de momentos de flexión



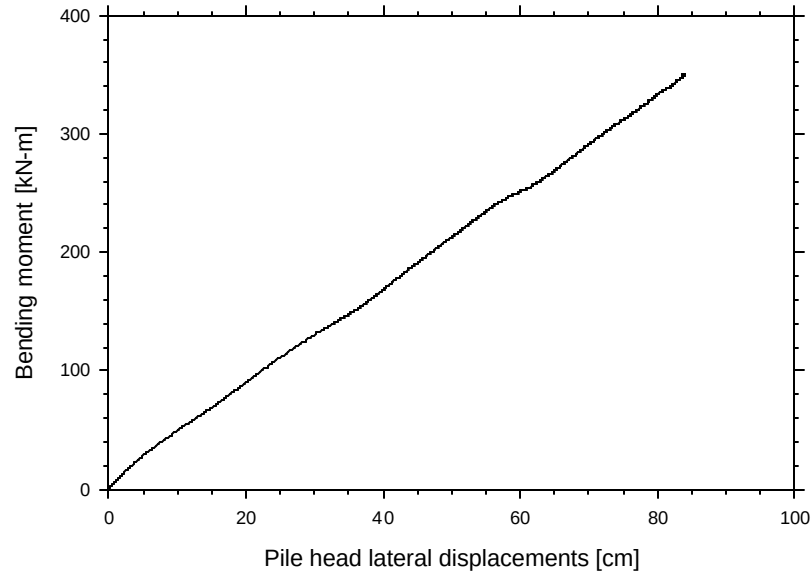
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Perfil de momentos de flexión



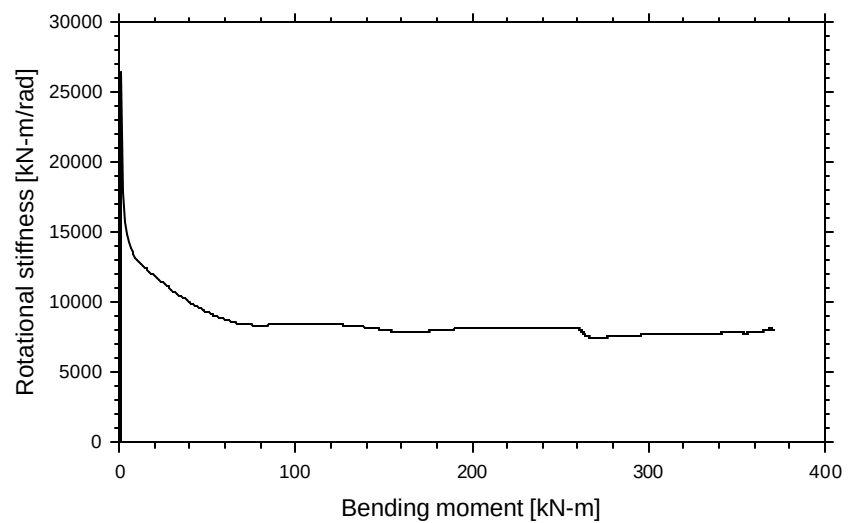
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Momento de flexión en la base del pilote vs desplazamiento lateral del pilote en la cabeza

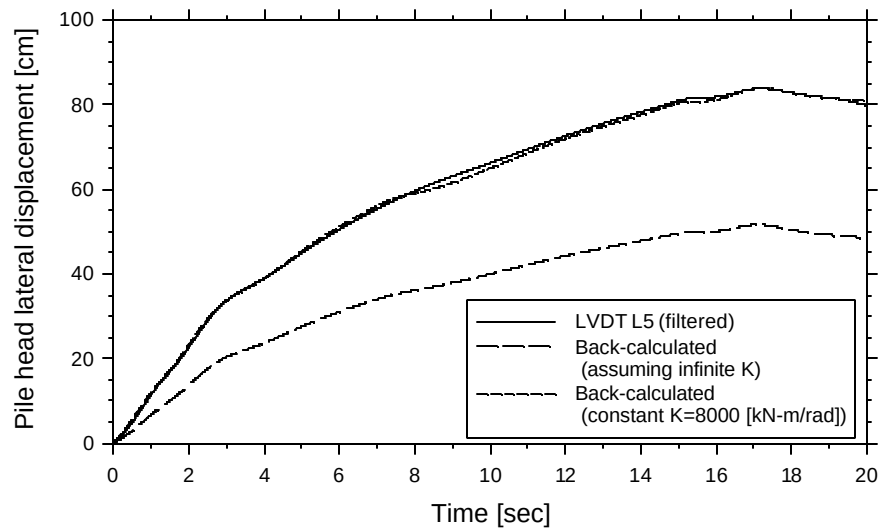


11

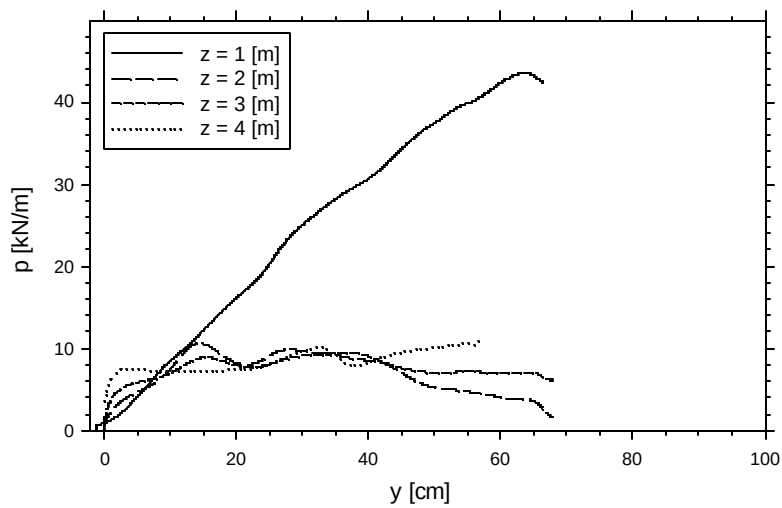
Rigidez rotacional de la arena cementada al rededor del pilote vs. momento de flexión en la base del estrato de arena licuada.



12

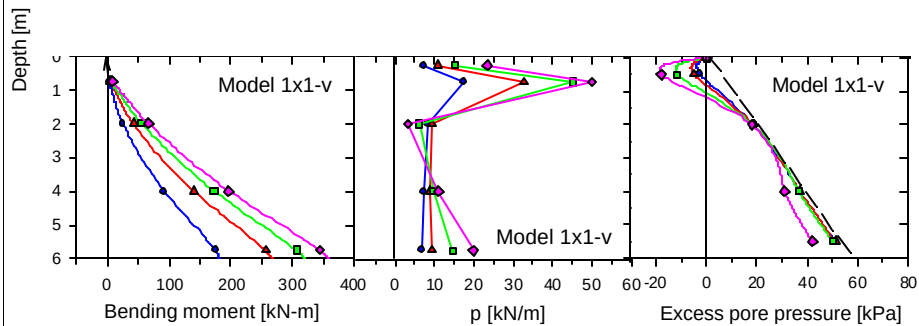
“Back-calculated” desplazamiento lateral de la cabeza del pilote

13

“Back-calculated” curvas p-y

14

Resumen de la respuesta del pilote aislado



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Vulnerability of highway bridges to lateral spreading

- Vulnerability of highway bridges to ground failures arising from liquefaction clearly demonstrated in past earthquakes, damage primarily associated to lateral spreading.
- Evaluation of lateral spreading involves considerable uncertainty; current state of practice utilizes Newmark approach.
- Once geometry of failure and magnitude of lateral deformation are estimated, an assessment should be made to see if the foundation is able to withstand the displacement demands.

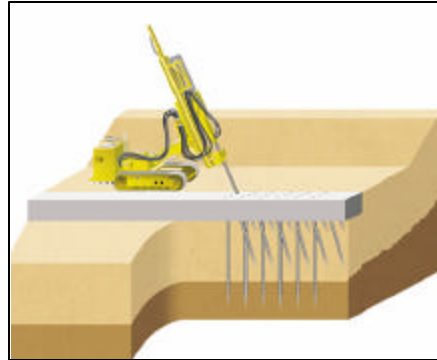


The Landing Road Bridge, after the 1987 New Zealand earthquake

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Pinning reinforcement effect on lateral spreading

- A refinement of the previous approach is to consider the reinforcing or pinning effects the piles have on the lateral stability.
- Lateral soil deformation may be reduced by restraining forces from pile foundations, expected loads imposed on piles can be smaller than those estimated without consideration of pile pinning effect..
- A series of four centrifuge tests were conducted to study the pinning effect the pile groups have on the lateral spreading. The centrifuge models simulate the case when a nonliquefied crust rides on top of a liquefied sand layer.



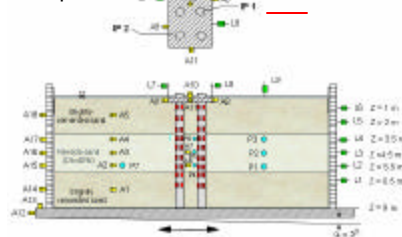
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Setup and instrumentation of centrifuge tests

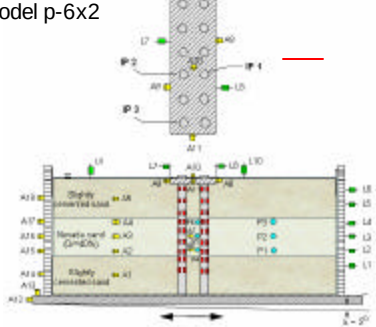
Model p-0



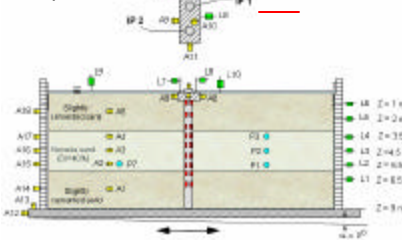
Model p-3x2



Model p-6x2

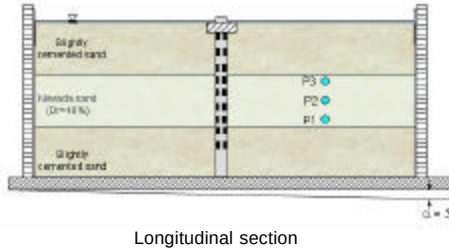
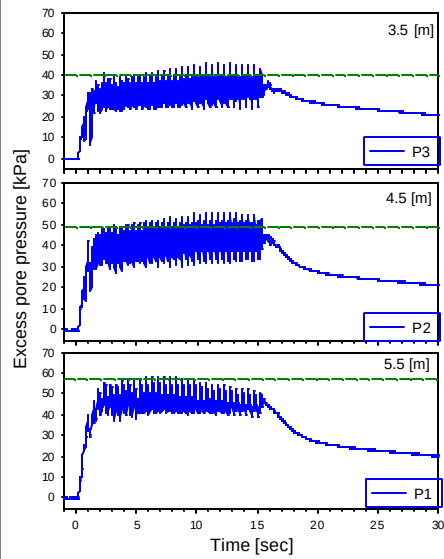


Model p-3x1



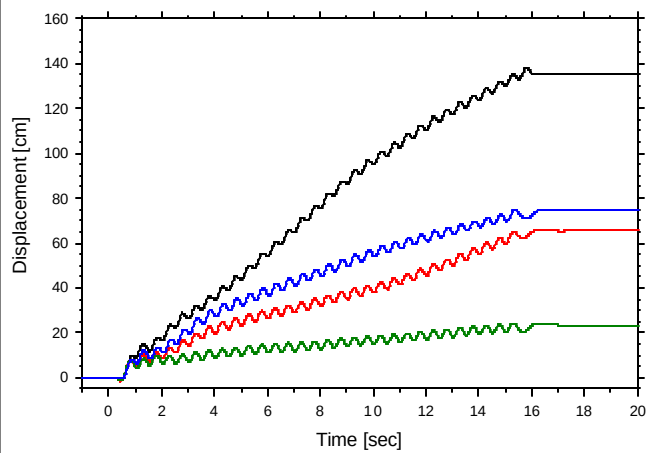
18

Excess pore pressure time histories, Model p-3x1

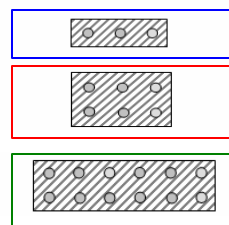


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Ground surface lateral displacements

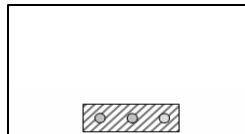
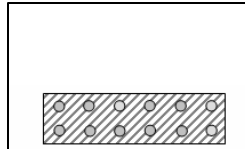
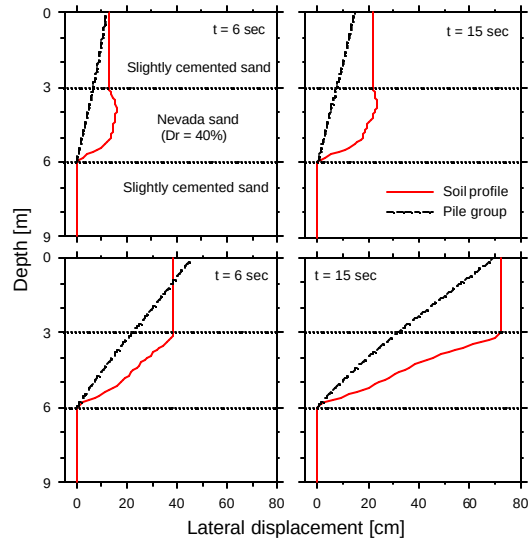


Free field



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Pile group and soil lateral displacement profiles



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Ground surface condition around pile groups

Model p-3x1



Free field disp. = 75 cm

Pile cap disp. = 67 cm

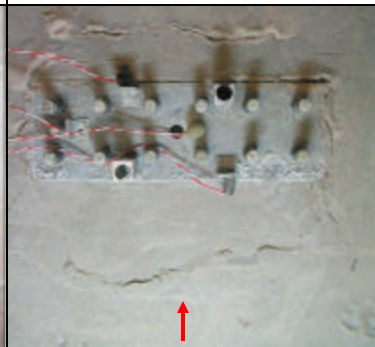
Model p-3x2



Free field disp. = 65 cm

Pile cap disp. = 43 cm

Model p-6x2

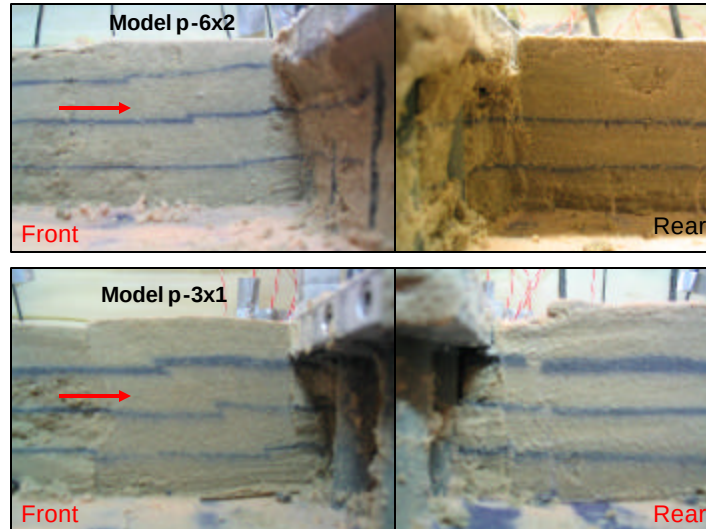


Free field disp. = 23 cm

Pile cap disp. = 15 cm

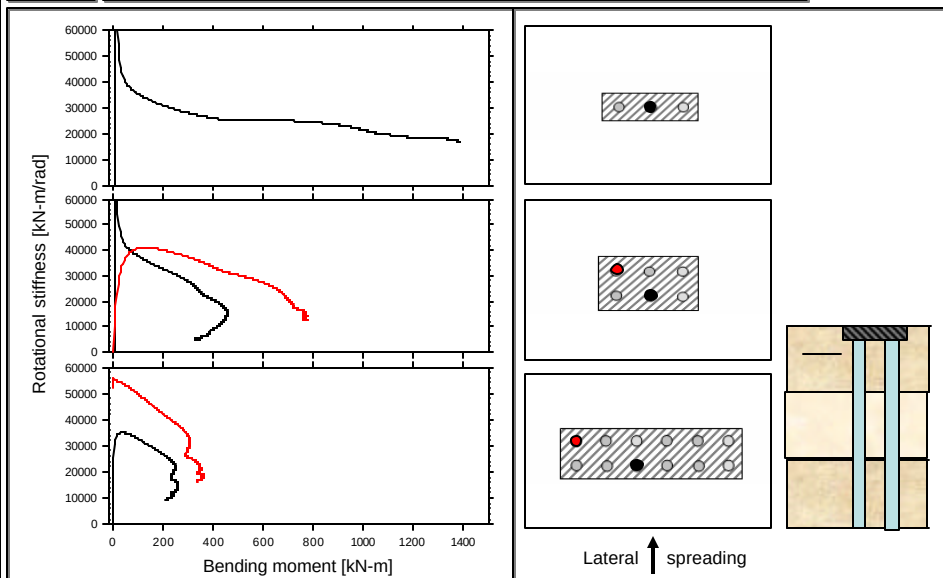
22

Passive failure in front of pile groups



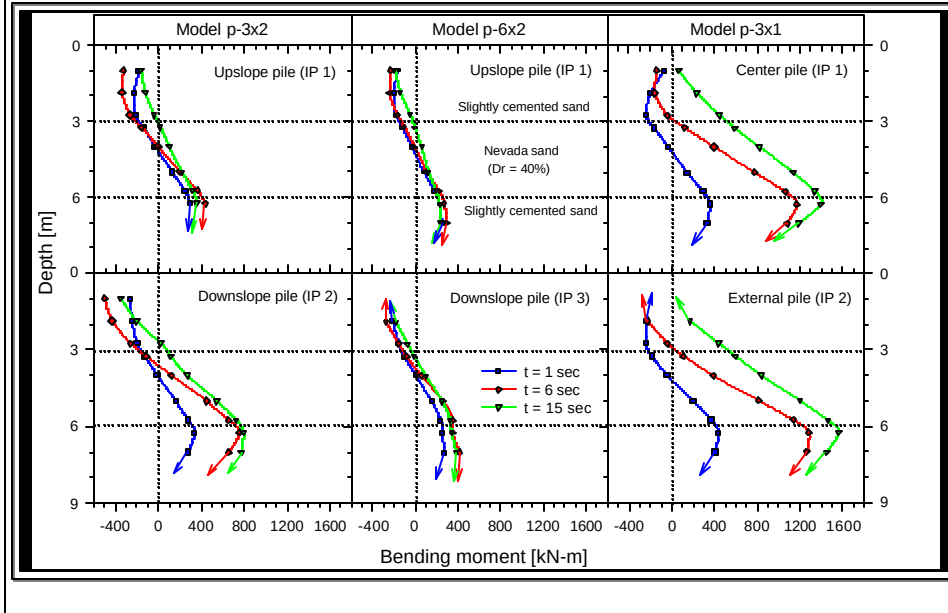
23

Rotational stiffness provided by the bottom cemented layer



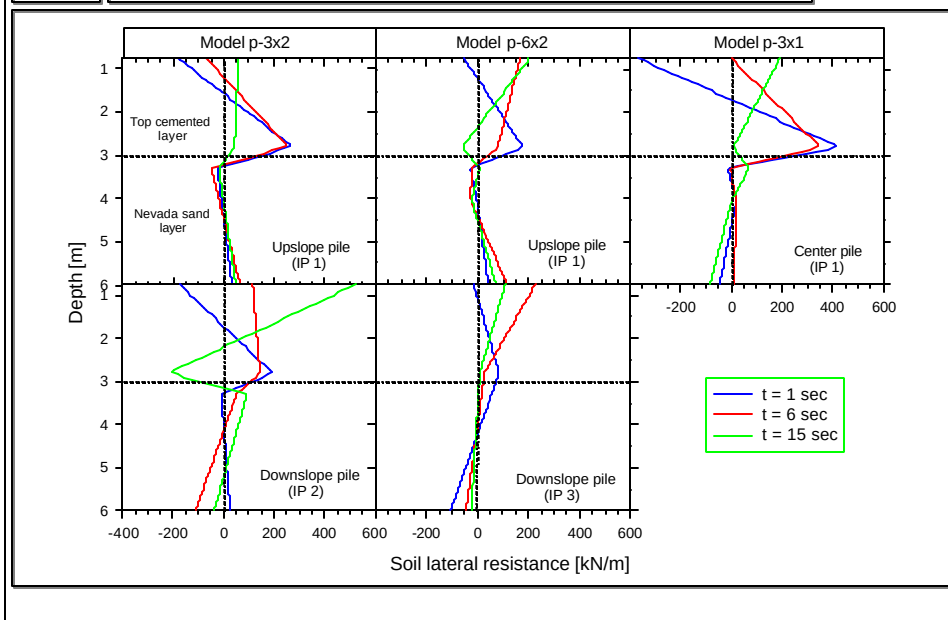
24

Summary of bending moment profiles



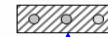
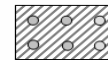
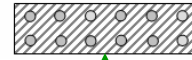
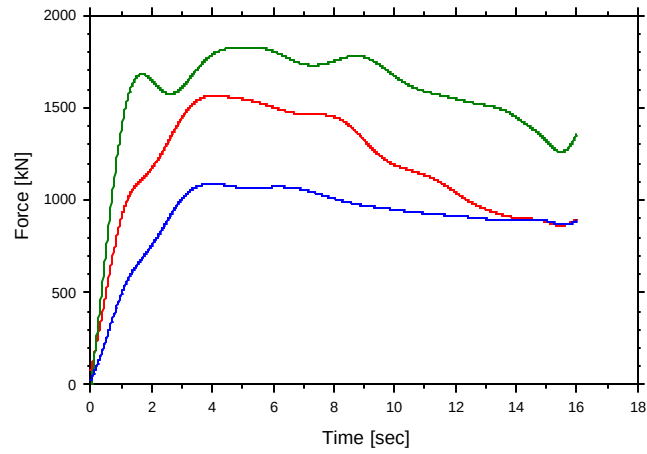
25

Lateral resistance against pile groups



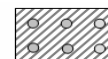
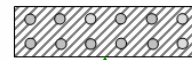
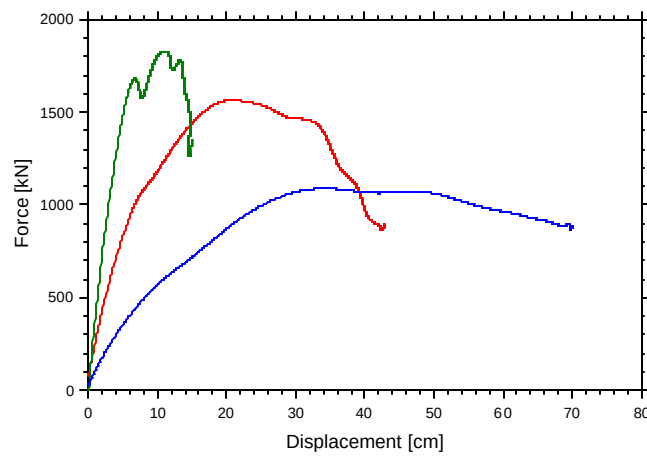
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Force time histories against pile groups



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Force versus pile group lateral displacement



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Normalized force versus pile group lateral displacement

