

Often large variations in values of strength of rock samples are attributed to sampling errors, accuracy of sample preparation or testing procedures e.g. platen constrain. Even when samples of identical lithological composition are tested, the existence of microscopic discontinuities results in variation in the value of mechanical properties, especially on the uniaxial compressive strength. Whilst it is widely accepted that discontinuities affect mechanical properties of rock and the existence of microcracks and their effect on sample failure propagation were investigated by numerous authors, (e.g. Farmer and Kemeny, 1992; Peng and Johnson, 1972; Horii and Nemat-Nasser, 1985), current laboratory testing practices and standards do not take into account the effects of these microscopic discontinuities on the mechanical properties of the rock.

Various modes of failure of cylindrical samples have been observed and classified (e.g. Reinhart, 1996; Paul and Gangal, 1996; Fairhurst and Cook, 1996). However, these observations were not considered when interpreting the results of uniaxial compressive strength tests. The relation between the mode of failure and strength parameters has not been investigated. Laboratory testing proved that fractures leading to sample failures are initiated on discontinuities. The location, orientation, size, density and extent of microscopic discontinuities contribute to different modes of failure of the rock sample (Szwedzicki and Shamu, 1999).

It is postulated that a common deficiency in assessment of the strength of the rock is that it does not take into account the mode of failure of the rock sample and rock mass. This could explain a large range of obtained values for relatively simple tests on rock samples.

2. Failure in Uniaxial Compression

Rock samples contain randomly oriented discontinuities. Under increasing uniaxial compression, stress in rock samples redistributes around such cracks. Sample failure is the result of microfracturing, the nucleation of cracks (tensile fractures of the microscopic scale) at points of stress concentration and their propagation along the direction of the maximum principal stress. Rock samples under uniaxial compressive stress, due to localised stress concentrations around microscopic discontinuities, can fail in tension, in shear or in coupling of the tension and shear stresses. Depending on the orientation of the cracks and the stress distribution, the failure is instigated in extension, shear or in coupling of shear and extension. The complete set of relations between the strain and stress components can be written in a matrix form. The matrix is known as the compliance matrix. The architecture of the elastic compliance matrix was illustrated conceptually by Hudson and Harrison (1997) as shown in Fig. 1.

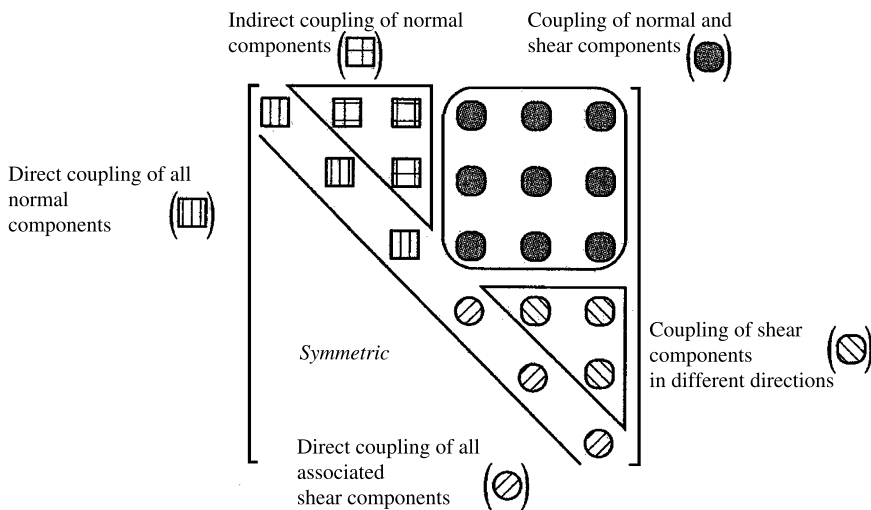


Fig. 1. The architecture of the elastic compliance matrix (Hudson and Harrison, 1997)

Two main categories of brittle fracture for a rock specimen subjected to uniaxial compression – axial cleavage and conjugate shear were identified (e.g. Gramberg, 1989). It was widely postulated that a mode of failure depended upon the degree of the end constraints of the sample offered by the platens of the testing machine and the surface quality of the parallel ends of the sample. Jumikis (1983) stated that the greater the friction between the platens and the specimen, the more likely it was that the sample would fail in shear.

The way the sample fails is reflected by the mode of the sample failure. This means that the mode of failure affects the resultant strength of the sample. Analysis of the mode of failure provides insights into the orientation of principal stress in rock samples. Extension fractures develop at right angle to the minimum principal compressive stress direction and will contain the orientation of the maximum and intermediate principal compressive stress.

The existence of microscopic discontinuities is responsible for “scale effects” i.e. strength reduction with increased sample size. The larger the sample the higher the probability that the discontinuities will effect the strength and that the sample will fail in a shear mode.

3. Matrix of Modes of Failure

The Uniaxial Compressive Strength (UCS) test “allows” a sample to choose the failure path and mode. For hard and brittle cylindrical rock samples five distinct modes of failure were identified by the author: simple extension, multiple extension, multiple fracturing, multiple shear, and simple shear, and are depicted in Fig. 2.

3.1 Simple Extension (Vertical Splitting, Axial Cleavage)

The simple extension mode denotes a failure along a plane parallel to the direction of compression. The simple extension failure doesn’t happen frequently and such a failure mode may suggest that the sample was relatively free of microscopic discontinuities.

3.2 Multiple Extension

Where two or more fractures run parallel to the long axis of the sample, with fracture(s) perpendicular to that direction, multiple extension failure takes place.

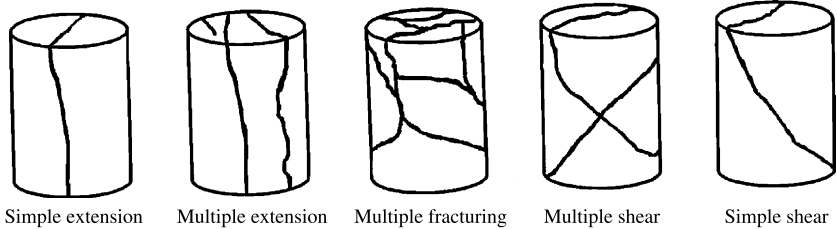


Fig. 2. Modes of sample failure

1 3.3 Multiple Fracturing

2 Multiple fracturing involves sample disintegration along a number of planes at various
3 angles. This type of failure of the specimen is often dynamic and violent with a large
4 amount of energy being released. When tensile failure is predominant, most of the
5 disintegration planes are in vertical and perpendicular directions to the loading force.
6 When shear forces are predominant, the sample disintegrates along planes inclined
7 and intersecting the mid height of the sample e.g. hour glassing or cone failure.

8 3.4 Multiple Shear

9 When fracturing takes place along two or more planes situated obliquely to the direction
10 of compression, but not being parallel to each other, the mode is called multiple shear.
11 The shear surfaces can be identified by the dust left behind when fracturing occurs.

12 3.5 Simple Shear

13 The single shear failure involves one or more major parallel shearing planes (zones)
14 situated at an oblique angle to the direction of maximum compression. The shear planes
15 usually develop across an unconfined part of the sample. Single shear may include shear
16 failure resulting from uneven loading of the sample. This happens when a single shear
17 commences from the top or bottom of the sample and progresses outwards. The max-
18 imum testing load for simple shear is often low compared with other failures since the
19 failure plane is often associated with a discontinuity or weak vein material.

20 It appears that rock samples in the uniaxial compressive test predominantly fail in
21 shear (simple or multiple).

22 Modes of failure can be classified similarly to the compliance matrix reflecting
23 various stress conditions, Fig. 3. However, it has to be noted that the theory of
24 elasticity does not apply to failure and there is no physical link between the elastic

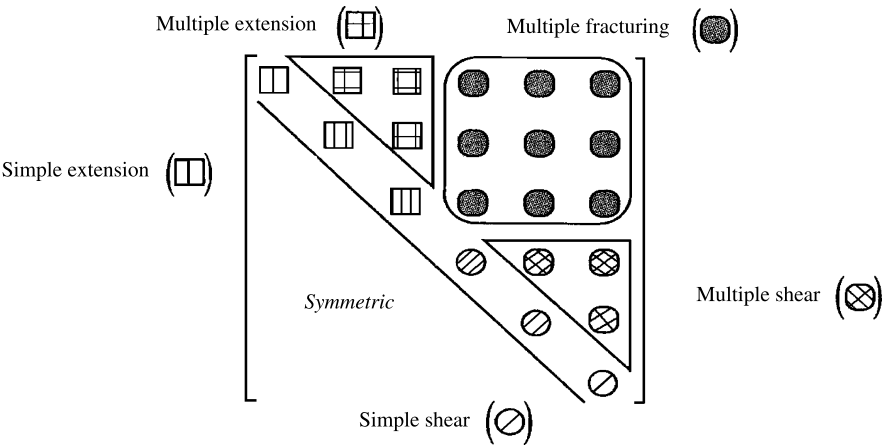


Fig. 3. The architecture of a matrix of failure modes of cylindrical rock samples tested in uniaxial compression



Fig. 4. A matrix form of failure modes of rock samples tested in uniaxial compression

compliance matrix and the matrix of failure modes. It can be argued that the value of compressive strength obtained when the rock failed in shear mode represented properties along the discontinuities, whereas the value obtained when the rock failed in extension mode represented strength of intact rock material.

Examples of cylindrical rock samples that failed in various modes were grouped in the matrix of modes of failure and are presented in Fig. 4.

It should be noted that during testing of rock samples from one geological formation, the mode of failure is usually similar for all samples due to the same type and orientation of defects that contribute to the same mode of failure.

4. Relation Between the Value of the UCS and the Mode of Failure

The results of UCS tests on rock samples are open for misinterpretation. The results of the UCS of rock samples show the coefficient of variation considerably higher than the results of the UCS of man made homogenous materials.

1 It is hypothesised that the results of tests on rock samples are not strictly compar-
2 able because tensile and shear components may vary in magnitude depending on the
3 mode of failure. The reason for this is principally due to discontinuities that affect the
4 modes of failure.

5 Szwedzicki and Shamu (1999) documented the effect of microscopic discontinu-
6 ities on the uniaxial compressive strength of cylindrical rock samples. To quantify the
7 effect of the mode of failure under uniaxial compression on the value of strength of
8 samples of different lithologies, a dimensionless parameter was introduced. The param-
9 eter was defined as the compressive strength normalised by the value of tensile
10 strength as defined by the Brazilian tensile test. The average value of this ratio was
11 lowest for single shear (6:1), slightly higher for multiple shear (10:1), higher for
12 multiple fracturing (15:1) and the highest for extension failure (20:1).

13 It is asserted that the variations in values of uniaxial compressive strength of
14 samples from the same lithology depends on the mode of failure. With the same mode
15 of failure, variations may be relatively small. However, when various modes of failure
16 take place on similar samples the variations can often reach extreme values. As an
17 example, four UCS tests on cylindrical contiguous samples of basalt that failed in
18 different modes are presented. The sample that failed in the simple shear mode had a
19 calculated UCS of 62 MPa. The sample which failed in the multiple shear mode had

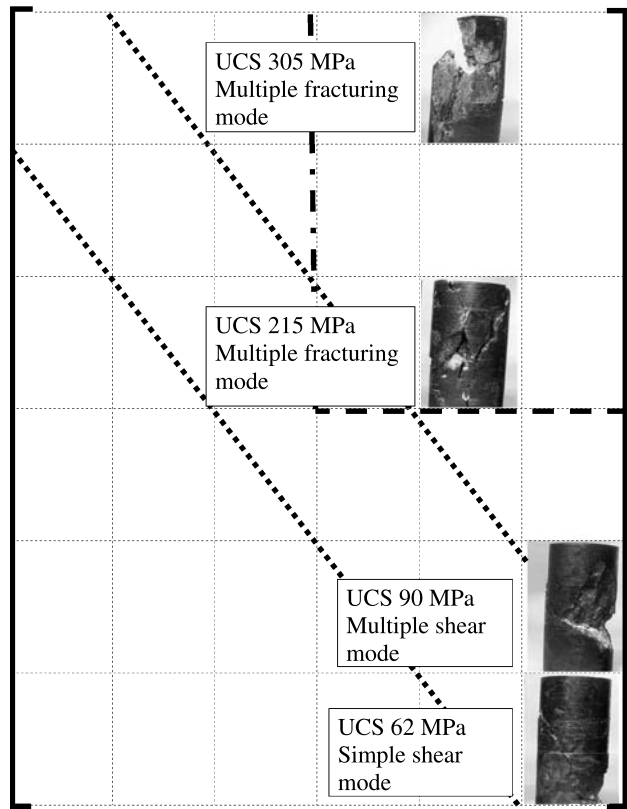


Fig. 5. Examples of values of the UCS of samples of basalt that failed in various modes

the UCS of 90 MPa. Two samples failed in the multiple fracturing mode. One sample that failed predominantly in shear stress had a UCS of 215 MPa and the other that failed predominantly in tensile stress had a UCS of 305 MPa. The value of the UCS and the positions of the samples in the mode matrix are shown in Fig. 5.

5. Conclusions

It appears that different modes of failure are due to the microscopic discontinuities in rock samples rather than variations in sample preparation, test procedure or end-boundary conditions.

It is postulated that analysis of the modes of failure makes it possible to determine whether the rock samples failed in tension, in shear or in coupling of tension and shear.

It is hypothesised that the way the sample fails (i.e. mode of failure) affects the obtained strength of rock samples. The value of the UCS is a function of the mode of failure – the values of the UCS obtained in extension are the highest, whilst the values obtained in shear are the lowest.

Understanding the affect of the mode of failure on strength enables an in-depth interpretation of the results of the Uniaxial Compressive Strength tests.

The hypothesis on the relationship between the modes of failure and strength of rock samples tested in uniaxial compression is presented to induce rock mechanics researchers to further research.

References

- Fairhurst, C., Cook, N. G. W. (1996): The phenomenon of rock splitting parallel to the direction of maximum compression in the neighbourhood of a surface. In: Proc., 1st Congress Int. Society Rock Mech, Lisbon, pp 687–692.
- Farmer, I. W., Kemeny, J. M. (1992): Deficiencies in rock test data. In: Proc., Int Symp. Eurock '92, London, pp 298–303.
- Gramberg, J. (1989): A non-conventional view on rock mechanics. Balkema, Rotterdam.
- Horii, H., Nemat-Nasser, S. (1985): Compression-induced microcrack growth in brittle solids: axial splitting and shear failure. *J. Geophys. Res.* 90(B4), 3105–3125.
- Hudson, J. A., Harrison, J. P. (1997): Engineering rock mechanics. Pergamon, Oxford.
- Jumikis, A. R. (1983): Rock mechanics, 2nd edn. Trans Tech Publ., Clausthal.
- Paul, B., Gangal, M. (1966): Initial and subsequent fracture curves for biaxial compression of brittle materials. In: Proc., 8th US Symposium on Rock Mechanics, Baltimore, 131–141.
- Peng, S., Johnson, A. M. (1972): Crack growth and faulting in cylindrical specimen of chemsford granite. In: *J. Rock Mech. Min. Sci.* 9, 37–86.
- Reinhart, J. S. (1966): Fracture of rocks. *Int. J. Fract. Mech.* 2, 534–590.
- Szwedzicki, T., Shamu, W. (1996): Detection of planes of weakness in rock samples using non-destructive testing method. In: Proc., '96 International Symposium on Mining Science and Technology, China. AA Balkema, Rotterdam, pp 759–763.
- Szwedzicki, T., Shamu, W. (1999): The effect of material discontinuities on strength of rock samples. In: Proc., Australasian Institute of Mining and Metallurgy. 304(1), 23–28.

Author's address: Tad Szwedzicki, 14 Gress brook Way, 6020 Carine, WA, Australia; e-mail: tadsz@iinet.net.au

Offprint Order

Journal: Rock Mechanics & Rock Engineering MS No.: TN/96 First Author: T. Szwedzicki

We will supply the corresponding author with one free copy of the relevant issue.

The order of offprints against payment must be sent in when returning the corrected proofs.

The prices quoted are valid only for authors ordering offprints for their private use.

Please write clearly in capital letters!

NEW When you order offprints against payment, you are entitled to receive in addition a pdf file of your article for your own personal use. As this pdf file is sent to you by e-mail, please insert the e-mail address here:

I hereby order against payment

☐ 50 ☐ 100 ☐ 200 ☐ 300 ☐ 400 offprints

Offprints should be sent to:

(Name of person or institution)

(Address)

Payment will be made by:

(Name of person or institution)

(Address)

(Purchase Order No.) _____ (Date/Signature of author) _____

☐ Please bill me **(please do not pay for offprints before receipt of invoice!)**

☐ Please charge my credit card ☐ Eurocard / Mastercard ☐ American Express
☐ Visa ☐ Diners Club

No.: _____ Valid until: _____

Signature: _____

(In all separate correspondence concerning this order please quote the Journal's title, MS No., and First Author.)

Price list for offprints*

Prices include carriage charges (surface mail). Prices are subject to change without notice.

***Customers in foreign EU countries:** Please state your V.A.T. registration number if applicable. Otherwise we have to add 10% V.A.T. to the list prices.

V.A.T. registration number: _____

Pages (Figs. incl./excl.)	50 Copies	100 Copies	200 Copies	300 Copies	400 Copies
	EUR	EUR	EUR	EUR	EUR
<input type="checkbox"/> 1-8	296,-	348,-	482,-	598,-	722,-
<input type="checkbox"/> 9-16	384,-	436,-	626,-	806,-	998,-
<input type="checkbox"/> 17-24	462,-	512,-	742,-	972,-	1198,-
<input type="checkbox"/> 25-32	512,-	564,-	844,-	1098,-	1408,-

Copyright Transfer Statement

The copyright to this article is hereby transferred to Springer (for US Government employees: to the extent transferable), effective if and when the article is accepted for publication. The copyright transfer covers the exclusive rights to reproduce and distribute the article, including reprints, photographic reproductions, microform, electronic database, videodiscs, or any other reproductions of similar nature, and translations.

However, the authors reserve:

1. All proprietary rights other than copyrights, such as patent rights.
2. The right to use all or part of this article in future works of their own and to grant or refuse permission to third parties to republish all or part of the article or translations thereof. To republish whole articles, such third parties must obtain written permission from Springer as well. However, Springer may grant rights concerning journal issues as a whole.

(Author's signature)

To be signed by at least one of the authors who agrees to inform the others, if any.

Instruction to printer	Mark	Examples	
		In the text	In the margin
Character to be corrected	/	Letter to be corrected	e /
Group of characters to be corrected	H	Letters to be corrected	ed H
Several identical characters to be corrected	/	Council for Commission	o ///
Differentiation of several errors in the same paragraph	/ F L J	There are many faults in this line	r / L m / i / a F
Character or word to be deleted	o	Commission and Parliament	o y o H
Character or word to be added	h	A word missing	is h
Superior character required	^	The Court's judgment.	(^) /
Omitted text to be added (see copy)	h	1. January h 12. December	h (Out see copy)
Inferior character required	v	H ₂ SO ₄	h /
Change to italic		Ad infinitum	(ital.)
Change italic characters to roman	O	status quo	(rom.)
Change capitals to lower case	O	UNESCO	(l.c.)
Change to capitals or small capitals	= =	Robert Burns, AD 1759-96	(Caps.) (S.C.)
Change to bold face	~~~~~	This word needs emphasising!	(bold)
To be letter-spaced		This text is too close	/
Correct horizontal alignment	==	This line is crooked	== /
Text to be raised or lowered	∩ ∪	This line is uneven	∩ / ∪ /
Text to be aligned (to the left)	⌋	This text is to be aligned	⌋ /
Text to be aligned (to the right)	⌈	This text is to be aligned	⌈ /
Text to be centred	[]	This text is to be centred	[] /
Take back to previous line]	This hyphen is unnecessary] /
Text to run on (no new paragraph)	~	... line. No new paragraph here	~ /
Take forward to next line	[This hyphen is badly placed	[/
Create new paragraph	⌋	... line. A new paragraph should begin here	⌋ /
Close up	o	A space is wrong here	o /
Equalise space	/	This spacing is very uneven	Y /
Add space between words	z	A space is missing here	z # /
Reduce space between words	z	These spaces are too big!	z /
Add space between lines	Y #	These lines are too close together	Y #
Reduce space between lines	Y	These lines are too far apart.	Y /
Stet (let original text stand)	⋮	This text was corrected in error	⊙
Transpose characters	S	These letters are transposed	S /
Transpose words	⌋	These are words transposed	⌋ /
Transpose lines	∩	These lines are transposed	∩ /

NB: A correction made in the text must always have a corresponding mark in the margin, otherwise it may be overlooked when the corrections are made. The same marks should be used, where appropriate, by copy-editors marking up copy. Where instructional words are used in marginal marks, e.g. 'ital.', 'bold', etc., they must always be encircled to show that they are not to be printed.

As a Springer-author you are now entitled to receive a 33,3 % price reduction on the list price of **all books** published by Springer Wien, Berlin/Heidelberg, New York, London, Paris, Barcelona, Tokyo and Hong Kong as well as Physica, Birkhäuser and Steinkopff. For your order please use this order form. Orders have to be sent directly to SpringerWienNewYork.

Als Autor/in von SpringerWienNewYork erhalten Sie 33,3% Rabatt auf den Ladenpreis der **gesamten Buchproduktion** von Springer Wien, Berlin/Heidelberg, New York, London, Paris, Barcelona, Tokyo und Hong Kong sowie der angeschlossenen Verlage Physica, Birkhäuser und Steinkopff. Bitte bestellen Sie mit diesem Bestellschein. Ihre Bestellung senden Sie bitte ausschließlich an SpringerWienNewYork.

For detailed information about titles published by SpringerWienNewYork please visit our homepage.
Nähere Informationen über das Programm von SpringerWienNewYork finden Sie auf unserer Homepage: **springer.at**

Springer, Order Department, P.O. Box 89, Sachsenplatz 4–6, 1201 Vienna, Austria, Fax +43.1.330 24 26
Springer, Auslieferung, Postfach 89, Sachsenplatz 4–6, 1201 Wien, Österreich, Fax +43.1.330 24 26

I order herewith / Ich bestelle hiermit:

[illegible]

Please copy this order form for your next orders. Bitte kopieren Sie diesen Bestellschein für Ihre weiteren Bestellungen.

- ☐ Please bill me / Bitte liefern Sie gegen Rechnung
- ☐ Please charge my credit card / Bitte belasten Sie meine Kreditkarte
- ☐ VISA ☐ MASTERCARD ☐ AMEX ☐ DINERS

Card No. / Karten-Nr.	Expiry date / Gültig bis
NAME / NAME		
ADDRESS / ADRESSE		
E-MAIL		
DATE / DATUM		
SIGNATURE / UNTERSCHRIFT		

CISM International Centre for Mechanical Sciences. Courses and Lectures

No. 486

Elso Kuljanic (ed.)
**AMST'05
Advanced Manufacturing
Systems and Technology**
Proceedings of the
International Conference
2005. XXII, 792 pages. 650 figures.
Softcover **EUR 108,-**
ISBN 3-211-26537-6

No. 483

Roger Grimshaw (ed.)
**Nonlinear Waves in Fluids:
Recent Advances and
Modern Applications**
2005. VII, 196 pages. 31 figures.
Softcover **EUR 50,-**
ISBN 3-211-25259-2

No. 481

C. G. Lai, K. Wilmski (eds.)
**Surface Waves in Geomechanics:
Direct and Inverse Modelling
for Soils and Rocks**
2005. V, 385 pp. 163 figs. With CD-Rom.
Softcover **EUR 80,-**
ISBN 3-211-27740-4

No. 480

L. Dormieux, F.-J. Ulm (eds.)
**Applied Micromechanics
of Porous Materials**
2005. V, 331 pages. 80 figures.
Softcover **EUR 75,-**
ISBN 3-211-26362-4

No. 479

V. Armenio, S. Sarkar (eds.)
Environmental Stratified Flows
2005. VII, 232 pages. 133 figures.
Softcover **EUR 60,-**
ISBN 3-211-28408-7

No. 474

Tomasz Sadowski (ed.)
**Multiscale Modelling
of Damage and
Fracture Processes
in Composite Materials**
2005. VII, 309 pages. 204 figures.
Softcover **EUR 76,-**
ISBN 3-211-29558-5

No. 473

Paolo B. Pascolo (ed.)
Biomechanics and Sports
Proceedings of the
XXI Winter Universiads 2003
2004. VII, 171 pages. 125 figures.
Softcover **EUR 49,-**
ISBN 3-211-21210-8

No. 470

M. Pignataro, V. Gioncu (eds.)
**Phenomenological
and Mathematical Modelling
of Structural Instabilities**
2005. VII, 336 pages. 270 figures.
Softcover **EUR 75,-**
ISBN 3-211-25292-4

No. 469

Z. Mróz, G. E. Stavroulakis (eds.)
**Parameter Identificaton
of Materials and Structures**
2005. VII, 340 pages. 180 figures.
Softcover **EUR 79,-**
ISBN 3-211-30151-8

No. 464

Helmut J. Böhm (eds.)
**Mechanics of Micro-
structured Materials**
2004. VII, 306 pages. 180 figures.
Softcover **EUR 72,50**
ISBN 3-211-24154-X

No. 455

J. Rondal, D. Dubina (eds.)
**Light Gauge Metal Structures
Recent Advances**
2005. VII, 253 pages. 168 figures.
Softcover **EUR 64,-**
ISBN 3-211-25258-4

No. 453

F. D. Fischer, E. Schmidt Inst. (eds.)
**Moving Interfaces
in Crystalline Solids**
2005. VIII, 256 pages. 126 figures.
Softcover **EUR 64,-**
ISBN 3-211-23899-9

No. 447

G. Del Piero, D. R. Owen (eds.)
**Multiscale Modeling in
Continuum Mechanics and
Structured Deformations**
2004. 275 pages. 61 figures.
Softcover **EUR 71,-**
ISBN 3-211-22425-4

No. 444

H. Irschik, K. Schlacher (eds.)
**Advanced Dynamics
and Control of Structures
and Machines**
2004. VII, 292 pages. 63 figures.
Softcover **EUR 70,-**
ISBN 3-211-22867-5

No. 416

Erwin Stein (ed.)
**Adaptive Finite Elements
in Linear and Nonlinear
Solid and Structural
Mechanics**
2005. V, 363 pages. 214 figures.
Softcover **EUR 82,-**
ISBN 3-211-26975-4

Recommended retail prices.
All prices are net-prices subject to local VAT.

33,3% cheaper for you ...

As a Springer-author you are now entitled to receive a 33,3% price reduction on the list price of **all books** published by Springer Wien, Berlin/Heidelberg, New York, London, Paris, Barcelona, Tokyo and Hong Kong as well as Physica, Birkhäuser and Steinkopff. For your order please use this order form. Orders have to be sent directly to SpringerWienNewYork.

Als Autor/in von SpringerWienNewYork erhalten Sie 33,3% Rabatt auf den Ladenpreis der **gesamten Buchproduktion** von Springer Wien, Berlin/Heidelberg, New York, London, Paris, Barcelona, Tokyo und Hong Kong sowie der angeschlossenen Verlage Physica, Birkhäuser und Steinkopff. Bitte bestellen Sie mit diesem Bestellschein. Ihre Bestellung senden Sie bitte ausschließlich an SpringerWienNewYork.

For detailed information about titles published by SpringerWienNewYork please visit our homepage.

Nähere Informationen über das Programm von SpringerWienNewYork finden Sie auf unserer Homepage: **springer.at**

Order Form / Bestellschein

Springer, Order Department, P.O. Box 89, Sachsenplatz 4–6, 1201 Vienna, Austria, Fax +43.1.330 24 26

Springer, Auslieferung, Postfach 89, Sachsenplatz 4–6, 1201 Wien, Österreich, Fax +43.1.330 24 26

I order herewith / Ich bestelle hiermit:

copy/ies	ISBN	Author	Title
Expl.	ISBN	Autor	Titel

Special Offer for Springer-Authors

Please copy this order form for your next orders. Bitte kopieren Sie diesen Bestellschein für Ihre weiteren Bestellungen.

☐ Please bill me / Bitte liefern Sie gegen Rechnung

☐ Please charge my credit card / Bitte belasten Sie meine Kreditkarte

☐ VISA ☐ MASTERCARD ☐ AMEX ☐ DINERS

Card No. / Karten-Nr. Expiry date / Gültig bis

NAME / NAME

ADDRESS / ADRESSE

E-MAIL

DATE / DATUM

SIGNATURE / UNTERSCHRIFT

**Bernhard Hofmann-Wellenhof,
Helmut Moritz**

Physical Geodesy

2005. XVII, 403 pages. 111 figures.
Softcover **EUR 59,-**. ISBN 3-211-23584-1

"Physical Geodesy" by Heiskanen and Moritz, published in 1967, has for a long time been considered as the standard introduction to its field. The enormous progress since then, however, required a complete reworking. While basic material could be retained other parts required a complete update. This concerns, above all, the adaptation to the fact that the geometry can now be precisely determined by methods such as GPS, and that new satellite methods, combined with terrestrial methods, also make a detailed determination of the earth's gravitational field a possibility and a necessity. Highlights include: emphasis on global integration of geometry and gravity, a simplified approach to Molodensky's theory without integral equations, and a general combination of all geodetic data by least-squares collocation.

**Bernhard Hofmann-Wellenhof,
Klaus Legat, Manfred Wieser**

Navigation

Principles of Positioning and Guidance

With a contribution by H. Lichtenegger.
2003. XXIX, 427 pages. 99 figures.
Softcover **EUR 59,90**. ISBN 3-211-00828-4

Global navigation satellite systems like GPS or the future European Galileo are influencing the world of navigation tremendously. Today, everybody is concerned with navigation even if unaware of this fact. Therefore, the interest in navigation is increasing.

This book provides an encyclopedic view of navigation. Fundamental elements are presented for a better understanding of the techniques, methods, and systems used in positioning and guidance.

The book is divided into three parts. Besides a historical review and maps, the first part covers mathematical and physical fundamentals. The second part treats the methods of positioning including terrestrial, celestial, satellite-based, inertial, image-based, and integrated navigation. Routing and guidance are the main topics of the third part.

**Bernhard Hofmann-Wellenhof,
Herbert Lichtenegger,
James Collins**

Global Positioning System

Theory and Practice

Fifth, revised edition.
2001. XXIII, 382 pages. 45 figures.
Softcover **EUR 62,95**. ISBN 3-211-83534-2

"... this book [is] an excellent standard reference on GPS for theoreticians and practitioners in the future."

Acta Geodaetica, Geophysica et Montanistica Hungarica

Gernot Beer (ed.)

Numerical Simulation in Tunnelling

2003. XVI, 477 pages. Numerous figures, partly in colour.
Hardcover **EUR 110,-**. ISBN 3-211-00515-3

The book presents the latest developments in the field of numerical simulation in tunneling. The work is a result of a five year joint research initiative of the Technical Universities of Graz and Vienna and the University of Innsbruck.

The book addresses tunneling practitioners as well as the academics involved in numerical modelling and / or tunnelling.

**Yong-Qi Chen,
Yuk-Cheung Lee (eds.)**

Geographical Data Acquisition

2001. XIV, 265 pages. 167 figures.
Softcover **EUR 69,95**. ISBN 3-211-83472-9

This book is dedicated to the theory and methodology of geographical data acquisition, providing comprehensive coverage ranging from the definition of geo-referencing systems, transformation between these systems to the acquisition of geographical data using different methods.

Recommended retail prices. Net-prices subject to local VAT.



SpringerWienNewYork

P.O. Box 89, Sachsenplatz 4-6, 1201 Vienna, Austria • Fax +43-1-330 24 26, books@springer.at, Internet: springer.at