

TORSION DE SAINT VENANT: ELEMENTO TRIANGULAR DE 6 NODOS EJE CIRCULAR CON RANURA

Coordenadas de los nodos

ORIGIN := 1

$$k := 1 \dots 61 \quad x_k := 0$$

$$i := 1 \dots 24 \quad y_k := 0$$

$$\alpha_i := (i - 1) \cdot \frac{\pi}{12}$$

$$x_i := \sin(\alpha_i) \quad y_i := -\cos(\alpha_i)$$

$$i := 1 \dots 12 \quad \alpha_i := (i - 1) \cdot \frac{\pi}{6} \quad x_{i+24} := \frac{\sin(\alpha_i)}{2} \quad y_{i+24} := \frac{-\cos(\alpha_i)}{2}$$

$$b := 2 \cdot \cos\left(\pi \cdot \frac{75}{180}\right) \quad b = 0.518$$

$$x_{18} := b \cdot \cos\left(37.5 \cdot \frac{\pi}{180}\right) - 1 \quad x_{18} = -0.589$$

$$y_{18} := b \cdot \sin\left(37.5 \cdot \frac{\pi}{180}\right) \quad y_{18} = 0.259$$

$$x_{19} := -0.482 \quad y_{19} := 0 \quad x_{20} := x_{18} \quad y_{20} := -y_{18} \quad x_{61} := 0 \quad y_{61} := 0$$

$$f(a,b) := \frac{a + b}{2}$$

$$x_{33} := f(x_{32}, x_{19}) \quad x_{34} := f(x_{61}, x_{19})$$

$$y_{33} := f(y_{32}, y_{19}) \quad y_{34} := f(y_{61}, y_{19})$$

$$x_{35} := f(x_{36}, x_{19}) \quad x_{37} := f(x_{25}, x_{19}) \quad x_{38} := f(x_3, x_{25}) \quad x_{39} := f(x_3, x_{27})$$

$$y_{35} := f(y_{36}, y_{19}) \quad y_{37} := f(y_{25}, y_{19}) \quad y_{38} := f(y_3, y_{25}) \quad y_{39} := f(y_3, y_{27})$$

$$x_{40} := f(x_5, x_{27}) \quad x_{41} := f(x_7, x_{27}) \quad x_{42} := f(x_7, x_{29}) \quad x_{43} := f(x_9, x_{29})$$

$$y_{40} := f(y_5, y_{27}) \quad y_{41} := f(y_7, y_{27}) \quad y_{42} := f(y_7, y_{29}) \quad y_{43} := f(y_9, y_{29})$$

$$x_{44} := f(x_{11}, x_{29})$$

$$x_{45} := f(x_{11}, x_{31})$$

$$x_{46} := f(x_{13}, x_{31})$$

$$x_{47} := f(x_{15}, x_{31})$$

$$y_{44} := f(y_{11}, y_{29})$$

$$y_{45} := f(y_{11}, y_{31})$$

$$y_{46} := f(y_{13}, y_{31})$$

$$y_{47} := f(y_{15}, y_{31})$$

$$x_{48} := f(x_{15}, x_{32})$$

$$x_{49} := f(x_{17}, x_{32})$$

$$x_{50} := f(x_{21}, x_{36})$$

$$x_{51} := f(x_{23}, x_{36})$$

$$y_{48} := f(y_{15}, y_{32})$$

$$y_{49} := f(y_{17}, y_{32})$$

$$y_{50} := f(y_{21}, y_{36})$$

$$y_{51} := f(y_{23}, y_{36})$$

$$x_{52} := f(x_{23}, x_{25})$$

$$x_{53} := f(x_{25}, x_{61})$$

$$x_{54} := f(x_{27}, x_{61})$$

$$x_{55} := f(x_{29}, x_{61})$$

$$y_{52} := f(y_{23}, y_{25})$$

$$y_{53} := f(y_{25}, y_{61})$$

$$y_{54} := f(y_{27}, y_{61})$$

$$y_{55} := f(y_{29}, y_{61})$$

$$x_{56} := f(x_{31}, x_{61})$$

$$x_{57} := f(x_{32}, x_{61})$$

$$x_{58} := f(x_{36}, x_{61})$$

$$x_{59} := f(x_{36}, x_{25})$$

$$y_{56} := f(y_{31}, y_{61})$$

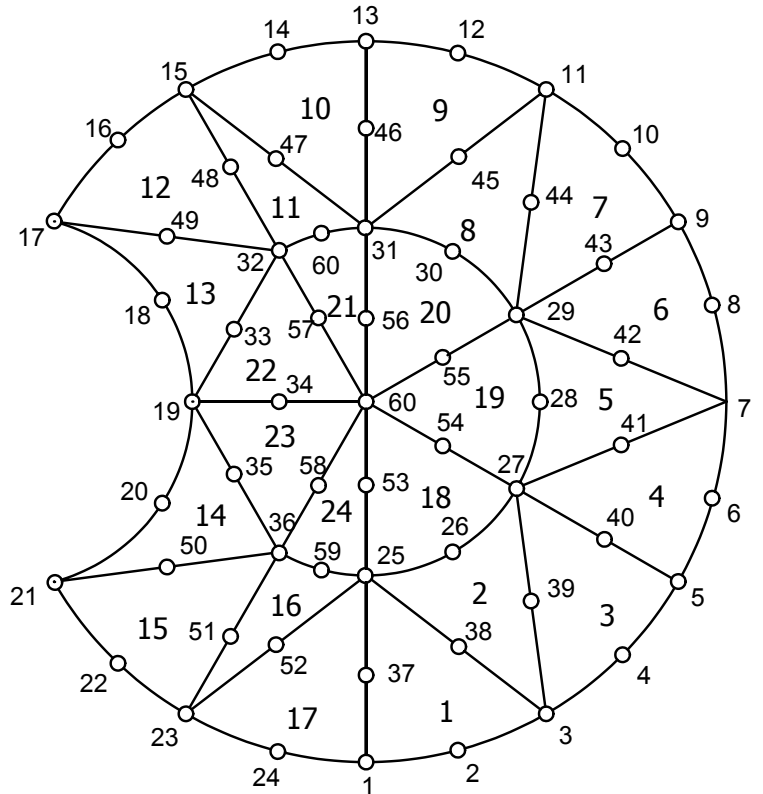
$$y_{57} := f(y_{32}, y_{61})$$

$$y_{58} := f(y_{36}, y_{61})$$

$$y_{59} := f(y_{36}, y_{25})$$

$$x_{60} := f(x_{32}, x_{31})$$

$$y_{60} := f(y_{32}, y_{31})$$



CONECTIVIDAD DE LOS ELEMENTOS

ii := 1 .. 48

kk := 1 .. 48

e := 1 .. 24 i := 1 .. 6

cc_{i,e} := 0

p := 1 .. 8

c_{i,p} := A1_{(p-1)·6+i}

p := 9 .. 16

c_{i,p} := A2_{(p-9)·6+i}

p := 17 .. 24

c_{i,p} := Au_{(p-17)·6+i}

A1_{ii} :=

1
3
25
2
38
37
3
27
25
39
26
38
3
5
27
4
40
39
5
7
27
6
41
40
7
29
27
42
28
41
7
9
29
8
43
42
9
11
29
10
44
43
11
31
29
45
30
44

A2_{ii} :=

11
13
31
12
46
45
13
15
31
14
47
46
5
32
31
48
60
47
15
17
32
16
49
48
17
19
32
18
33
49
19
21
36
20
50
35
21
23
36
22
51
50
23
25
36
52
59
51

Au_{kk} :=

23
1
25
24
37
52
25
27
61
26
54
53
27
29
61
28
55
54
29
31
61
30
56
55
31
32
61
60
57
56
32
19
61
33
34
57
19
36
61
35
58
34
36
25
61
59
53
58

$$c = \begin{pmatrix} 1 & 3 & 3 & 5 & 7 & 7 & 9 & 11 & 11 & 13 & 5 & 15 & 17 & 19 & 21 & 23 & 23 & 25 & 27 & 29 & 31 & 32 & 19 & 36 \\ 3 & 27 & 5 & 7 & 29 & 9 & 11 & 31 & 13 & 15 & 32 & 17 & 19 & 21 & 23 & 25 & 1 & 27 & 29 & 31 & 32 & 19 & 36 & 25 \\ 25 & 25 & 27 & 27 & 27 & 29 & 29 & 29 & 31 & 31 & 31 & 32 & 32 & 36 & 36 & 36 & 25 & 61 & 61 & 61 & 61 & 61 & 61 & 61 \\ 2 & 39 & 4 & 6 & 42 & 8 & 10 & 45 & 12 & 14 & 48 & 16 & 18 & 20 & 22 & 52 & 24 & 26 & 28 & 30 & 60 & 33 & 35 & 59 \\ 38 & 26 & 40 & 41 & 28 & 43 & 44 & 30 & 46 & 47 & 60 & 49 & 33 & 50 & 51 & 59 & 37 & 54 & 55 & 56 & 57 & 34 & 58 & 53 \\ 37 & 38 & 39 & 40 & 41 & 42 & 43 & 44 & 45 & 46 & 47 & 48 & 49 & 35 & 50 & 51 & 52 & 53 & 54 & 55 & 56 & 57 & 34 & 58 \end{pmatrix}$$

FUNCIONES DE INTERPOLACION

Coordenadas naturales de los nodos -->

$$\xi := \begin{pmatrix} 1 \\ 0 \\ 0 \\ \frac{1}{2} \\ 0 \\ \frac{1}{2} \end{pmatrix} \quad \eta := \begin{pmatrix} 0 \\ 1 \\ 0 \\ \frac{1}{2} \\ \frac{1}{2} \\ 0 \end{pmatrix}$$

$$N_{1,i} := \xi_i (2 \cdot \xi_i - 1)$$

$$N_{2,i} := \eta_i (2 \cdot \eta_i - 1)$$

$$N_{3,i} := (1 - \xi_i - \eta_i) [2 \cdot (1 - \xi_i - \eta_i) - 1]$$

$$N_{4,i} := 4 \cdot \xi_i \cdot \eta_i$$

$$N_{5,i} := 4 \cdot \eta_i (1 - \xi_i - \eta_i)$$

$$N_{6,i} := 4 \cdot \xi_i (1 - \xi_i - \eta_i)$$

Comprobación:

$$N = \begin{pmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix}$$

COORDENADAS DE LOS PUNTOS DE LA INTEGRACION DE GAUSS

$$\xi := \begin{pmatrix} 0.8168475730 \\ 0.0915762135 \\ 0.0915762135 \\ 0.1081030182 \\ 0.4459484909 \\ 0.4459484909 \end{pmatrix} \quad \eta := \begin{pmatrix} 0.0915762135 \\ 0.8168475730 \\ 0.0915762135 \\ 0.4459484909 \\ 0.1081030182 \\ 0.4459484909 \end{pmatrix}$$

EVALUACION DE LAS FUNCIONES DE INTERPOLACION

$$N_{1,i} := \xi_i (2 \cdot \xi_i - 1)$$

$$N_{2,i} := \eta_i (2 \cdot \eta_i - 1)$$

$$N_{3,i} := (1 - \xi_i - \eta_i) [2 \cdot (1 - \xi_i - \eta_i) - 1]$$

$$N_{4,i} := 4 \cdot \xi_i \cdot \eta_i$$

$$N_{5,i} := 4 \cdot \eta_i (1 - \xi_i - \eta_i)$$

$$N_{6,i} := 4 \cdot \xi_i (1 - \xi_i - \eta_i)$$

DERIVADAS DE LAS FUNCIONES DE INTERPOLACION

$$N\xi_{1,i} := 4 \cdot \xi_i - 1$$

$$N\eta_{1,i} := 0$$

$$N\xi_{2,i} := 0$$

$$N\eta_{2,i} := 4 \cdot \eta_i - 1$$

$$N\xi_{3,i} := -3 + 4 \cdot \eta_i + 4 \cdot \xi_i$$

$$N\eta_{3,i} := -3 + 4 \cdot \xi_i + 4 \cdot \eta_i$$

$$N\xi_{4,i} := 4 \cdot \eta_i$$

$$N\eta_{4,i} := 4 \cdot \xi_i$$

$$N\xi_{5,i} := -4 \cdot \eta_i$$

$$N\eta_{5,i} := 4 - 8 \cdot \eta_i - 4 \cdot \xi_i$$

$$N\xi_{6,i} := 4 - 8 \cdot \xi_i - 4 \cdot \eta_i$$

$$N\eta_{6,i} := -4 \cdot \xi_i$$

COEFICIENTES DE GAUSS

$$W_i :=$$

0.05497587185
0.05497587185
0.05497587185
0.11169079485
0.11169079485
0.11169079485

JACOBIANOS PARA LOS PUNTOS DE INTEGRACION

$$j := 1 \dots 6$$

$$J_{11,i,e} := \sum_j N_{\xi,j,i} x(c_{j,e}) \quad J_{12,i,e} := \sum_j N_{\xi,j,i} y(c_{j,e})$$

$$J_{21,i,e} := \sum_j N_{\eta,j,i} x(c_{j,e}) \quad J_{22,i,e} := \sum_j N_{\eta,j,i} y(c_{j,e})$$

DETERMINANTE DEL JACOBIANO

$$\det J_{i,e} := J_{11,i,e} \cdot J_{22,i,e} - J_{12,i,e} \cdot J_{21,i,e}$$

MATRIZ T

$$\text{T11}_{i,e} := \left(\text{J22}_{i,e} \right)^2 + \left(\text{J21}_{i,e} \right)^2$$

$$T12_{i,e} := -(J12_{i,e} \cdot J22_{i,e} + J11_{i,e} \cdot J21_{i,e})$$

$$T22_{i,e} := (J11_{i,e})^2 + (J12_{i,e})^2$$

$$T21_{i,e} := T12_{i,e}$$

MATRIZ T_xN,

$$Q^1_{(e-1) \cdot 6 + i, j} := T11_{i, e} \cdot N^{\xi}_{j, i} + T12_{i, e} \cdot N^{\eta}_{j, i}$$

$$Q2_{(e-1) \cdot 6+i,j} := T21_{i,e} \cdot N\xi_{j,i} + T22_{i,e} \cdot N\eta_{j,i}$$

MATRIZ K

$$k := 1 \dots 6$$

$$K_{(e-1) \cdot 6+k, j} := \sum_i \frac{W_i}{\det J_{i, e}} \left[N_{k, i}^{z_1} Q_{(e-1) \cdot 6+i, j}^1 + N_{k, i}^{\eta} Q_{(e-1) \cdot 6+i, j}^2 \right]$$

VECTOR DE FUERZAS EXTERNAS

$$P_{j,e} := 2 \cdot \sum_i W_i \cdot \det J_{i,e} \cdot N_{j,i}$$

FORMACION DE LA MATRIZ GLOBAL Y EL VECTOR DE CARGAS

$$\text{Kt}_{c_i, e, c_j, e} := 0 \qquad F_{c_i, e} := 0$$

$$\mathbf{Kt}_{c_i, e, c_j, e} := \mathbf{Kt}_{c_i, e, c_j, e} + \mathbf{K}_{(e-1) \cdot 6 + i, j}$$

$$F_{c_i,e} := F_{c_i,e} + P_{i,e}$$

CONDICIONES DE BORDE Y SOLUCION PARA LA FUNCION DE PRANDTL

$$k := 1 \dots 24$$

$$K_{t_{k,k}} := 10^{10}$$

SOLUCION PARA LA FUNCION INCOGNITA

$$\mathbf{F_i} := \mathbf{K_t}^{-1} \cdot \mathbf{F}$$

CALCULO DE J (dos veces el volumen bajo la superficie fi)

$$\text{Vol} := \sum_e \sum_j \sum_i W_i \cdot \det J_{i,e} \cdot N_{j,i} \cdot \text{Fi}(c_{j,e}) \quad 2 \cdot \text{Vol} = 1.061$$

[illegible]

DETERMINACION DE LAS TENSIONES EN LOS NODOS

Coordenadas de los nodos:

$$\xi := \begin{pmatrix} 1 \\ 0 \\ 0 \\ \frac{1}{2} \\ 0 \\ \frac{1}{2} \end{pmatrix} \quad \eta := \begin{pmatrix} 0 \\ 1 \\ 0 \\ \frac{1}{2} \\ \frac{1}{2} \\ 0 \end{pmatrix}$$

Derivadas de las funciones de forma:

$$\begin{aligned} N\xi_{1,i} &:= 4 \cdot \xi_i - 1 & N\eta_{1,i} &:= 0 \\ N\xi_{2,i} &:= 0 & N\eta_{2,i} &:= 4 \cdot \eta_i - 1 \\ N\xi_{3,i} &:= -3 + 4 \cdot \eta_i + 4 \cdot \xi_i & N\eta_{3,i} &:= -3 + 4 \cdot \xi_i + 4 \cdot \eta_i \\ N\xi_{4,i} &:= 4 \cdot \eta_i & N\eta_{4,i} &:= 4 \cdot \xi_i \\ N\xi_{5,i} &:= -4 \cdot \eta_i & N\eta_{5,i} &:= 4 - 8 \cdot \eta_i - 4 \cdot \xi_i \\ N\xi_{6,i} &:= 4 - 8 \cdot \xi_i - 4 \cdot \eta_i & N\eta_{6,i} &:= -4 \cdot \xi_i \end{aligned}$$

Elementos del Jacobiano:

$$\begin{aligned} J11_{i,e} &:= \sum_j N\xi_{j,i} \cdot x(c_{j,e}) & J12_{i,e} &:= \sum_j N\xi_{j,i} \cdot y(c_{j,e}) \\ J21_{i,e} &:= \sum_j N\eta_{j,i} \cdot x(c_{j,e}) & J22_{i,e} &:= \sum_j N\eta_{j,i} \cdot y(c_{j,e}) \end{aligned}$$

Determinante del Jacobiano:

$$\det J_{i,e} := J11_{i,e} \cdot J22_{i,e} - J12_{i,e} \cdot J21_{i,e}$$

Derivada de la función de Prandtl respecto a x en el nodo i del elemento e:

$$Fix_{i,e} := \frac{1}{\det J_{i,e}} \cdot \left[J22_{i,e} \cdot \sum_j N\xi_{j,i} \cdot Fi(c_{j,e}) - J12_{i,e} \cdot \sum_j N\eta_{j,i} \cdot Fi(c_{j,e}) \right]$$

Derivada de la función de Prandtl respecto a y en el nodo i del elemento e:

$$Fiy_{i,e} := \frac{1}{\det J_{i,e}} \cdot \left[(-J21)_{i,e} \cdot \sum_j N\xi_{j,i} \cdot Fi(c_{j,e}) + J11_{i,e} \cdot \sum_j N\eta_{j,i} \cdot Fi(c_{j,e}) \right]$$

0
0
0
0
0
0.297
0.321
0.33
0.335
0.334
0.334
Fi = 0.337
0.279
0.175
0.258
0.165
0.245
0.184
0.205
0.211
0.201
0.216
0.216
0.203
0.215
0.212
0.183
0.124
0.126
0.083
0.082
0.148
0.177
0.357
0.395
0.4
0.373
0.334
0.319
0.282
0.324
(0.375)

conectividada -->

$$c = \begin{pmatrix} 1 & 3 & 3 & 5 & 7 & 7 & 9 & 11 & 11 & 13 & 5 & 15 & 17 & 19 & 21 & 23 & 23 & 25 & 27 & 29 & 31 & 32 & 19 & 36 \\ 3 & 27 & 5 & 7 & 29 & 9 & 11 & 31 & 13 & 15 & 32 & 17 & 19 & 21 & 23 & 25 & 1 & 27 & 29 & 31 & 32 & 19 & 36 & 25 \\ 25 & 25 & 27 & 27 & 27 & 29 & 29 & 29 & 31 & 31 & 31 & 32 & 32 & 36 & 36 & 36 & 25 & 61 & 61 & 61 & 61 & 61 & 61 & 61 \\ 2 & 39 & 4 & 6 & 42 & 8 & 10 & 45 & 12 & 14 & 48 & 16 & 18 & 20 & 22 & 52 & 24 & 26 & 28 & 30 & 60 & 33 & 35 & 59 \\ 38 & 26 & 40 & 41 & 28 & 43 & 44 & 30 & 46 & 47 & 60 & 49 & 33 & 50 & 51 & 59 & 37 & 54 & 55 & 56 & 57 & 34 & 58 & 53 \\ 37 & 38 & 39 & 40 & 41 & 42 & 43 & 44 & 45 & 46 & 47 & 48 & 49 & 35 & 50 & 51 & 52 & 53 & 54 & 55 & 56 & 57 & 34 & 58 \end{pmatrix}$$

$$\text{Fix}^T = \begin{pmatrix} -0.004 & -0.459 & 0.083 & -0.226 & -0.16 & 0.002 \\ -0.474 & -0.313 & 0.096 & -0.489 & -0.085 & -0.122 \\ -0.457 & -0.818 & -0.314 & -0.633 & -0.548 & -0.424 \\ -0.822 & -0.94 & -0.316 & -0.881 & -0.645 & -0.588 \\ -0.937 & -0.327 & -0.317 & -0.673 & -0.322 & -0.668 \\ -0.938 & -0.828 & -0.328 & -0.883 & -0.597 & -0.65 \\ -0.824 & -0.467 & -0.328 & -0.643 & -0.438 & -0.558 \\ -0.432 & -0.03 & -0.305 & -0.177 & -0.176 & -0.466 \\ -0.448 & -0.003 & 0.081 & -0.213 & 0.022 & -0.167 \\ 0.003 & 0.141 & 0.618 & 0.131 & 0.398 & 0.315 \\ -0.206 & 0.437 & 0.034 & 0.031 & 0.235 & -0.188 \\ 0.225 & 0.081 & 0.786 & 0.177 & 0.439 & 0.485 \\ 0.129 & 1.628 & 0.809 & 0.801 & 1.068 & 0.478 \\ 1.603 & 0.202 & 0.641 & 0.842 & 0.417 & 0.943 \\ 0.128 & 0.352 & 0.665 & 0.278 & 0.523 & 0.399 \\ 0.398 & 0.124 & 0.408 & 0.261 & 0.266 & 0.403 \\ 0.36 & 0.004 & 0.143 & 0.2 & 0.107 & 0.235 \\ 0.097 & -0.354 & 0.277 & -0.094 & -0.003 & 0.137 \\ -0.359 & -0.382 & 0.301 & -0.371 & -0.086 & -0.073 \\ -0.372 & -0.024 & 0.286 & -0.152 & 0.079 & -0.004 \\ 0.022 & 0.492 & 0.377 & 0.257 & 0.434 & 0.2 \\ 0.544 & 1.367 & 0.19 & 0.955 & 0.778 & 0.367 \\ 1.367 & 0.505 & 0.19 & 0.936 & 0.348 & 0.778 \\ 0.423 & 0.12 & 0.388 & 0.272 & 0.254 & 0.406 \end{pmatrix}$$

$$\text{Fiy}^T = \begin{pmatrix} 0.88 & 0.802 & 0.309 & 0.844 & 0.594 & 0.594 \\ 0.781 & 0.206 & 0.327 & 0.483 & 0.28 & 0.645 \\ 0.783 & 0.477 & 0.206 & 0.633 & 0.373 & 0.49 \\ 0.47 & 0.004 & 0.201 & 0.236 & 0.141 & 0.304 \\ -0.002 & -0.193 & 0.201 & -0.19 & 0.007 & 0.194 \\ -0.004 & -0.474 & -0.195 & -0.237 & -0.303 & -0.137 \\ -0.481 & -0.802 & -0.196 & -0.643 & -0.495 & -0.37 \\ -0.806 & -0.403 & -0.199 & -0.678 & -0.296 & -0.492 \\ -0.783 & -0.791 & -0.555 & -0.794 & -0.673 & -0.691 \\ -0.791 & -0.247 & -0.555 & -0.488 & -0.375 & -0.673 \\ -0.156 & 0.206 & -0.259 & 0.337 & -0.027 & 0.174 \\ -0.386 & -0.048 & -0.322 & -0.177 & -0.132 & -0.365 \\ 0.389 & 0.097 & -0.112 & 0.615 & 0.073 & 0.219 \\ -0.095 & -0.61 & 0.167 & -0.646 & -0.178 & -0.06 \\ 0.075 & 0.603 & -0.059 & 0.278 & 0.264 & -0.014 \\ 0.576 & 0.334 & 0.089 & 0.455 & 0.212 & 0.333 \\ 0.629 & 0.88 & 0.309 & 0.745 & 0.594 & 0.492 \\ 0.32 & 0.232 & -0.008 & 0.296 & 0.173 & 0.156 \\ 0.224 & -0.222 & 0.033 & 0.007 & -0.015 & 0.052 \\ -0.24 & -0.214 & 0.06 & -0.254 & -0.077 & -0.159 \\ -0.214 & -0 & 0.06 & -0.107 & 0.03 & -0.077 \\ 0.03 & 0.237 & -0.048 & 0.134 & 0.094 & -0.009 \\ -0.222 & 0.094 & 0.106 & -0.064 & 0.1 & -0.058 \\ 0.142 & 0.32 & -0.008 & 0.231 & 0.156 & 0.067 \end{pmatrix}$$

Módulo de la tensión:

$$\tau_{i,e} := \sqrt{\left(\text{Fix}_{i,e}\right)^2 + \left(\text{Fiy}_{i,e}\right)^2}$$

$$\tau^T = \begin{pmatrix} 0.88 & 0.924 & 0.32 & 0.874 & 0.615 & 0.594 \\ 0.914 & 0.375 & 0.341 & 0.687 & 0.293 & 0.657 \\ 0.907 & 0.947 & 0.375 & 0.895 & 0.663 & 0.648 \\ 0.947 & 0.94 & 0.375 & 0.912 & 0.66 & 0.662 \\ 0.937 & 0.38 & 0.375 & 0.699 & 0.322 & 0.696 \\ 0.938 & 0.954 & 0.382 & 0.914 & 0.669 & 0.664 \\ 0.954 & 0.928 & 0.382 & 0.909 & 0.66 & 0.669 \\ 0.914 & 0.404 & 0.364 & 0.701 & 0.344 & 0.677 \\ 0.902 & 0.791 & 0.561 & 0.822 & 0.673 & 0.711 \\ 0.791 & 0.285 & 0.83 & 0.505 & 0.547 & 0.743 \\ 0.258 & 0.483 & 0.261 & 0.339 & 0.237 & 0.256 \\ 0.446 & 0.094 & 0.849 & 0.251 & 0.459 & 0.607 \\ 0.41 & 1.631 & 0.816 & 1.01 & 1.071 & 0.525 \\ 1.606 & 0.643 & 0.662 & 1.061 & 0.453 & 0.945 \\ 0.148 & 0.698 & 0.668 & 0.393 & 0.585 & 0.399 \\ 0.7 & 0.357 & 0.418 & 0.525 & 0.34 & 0.523 \\ 0.725 & 0.88 & 0.34 & 0.771 & 0.604 & 0.545 \\ 0.334 & 0.424 & 0.277 & 0.311 & 0.173 & 0.208 \\ 0.423 & 0.442 & 0.303 & 0.371 & 0.088 & 0.09 \\ 0.442 & 0.216 & 0.292 & 0.296 & 0.11 & 0.159 \\ 0.215 & 0.492 & 0.382 & 0.278 & 0.435 & 0.214 \\ 0.545 & 1.387 & 0.196 & 0.965 & 0.784 & 0.367 \\ 1.384 & 0.514 & 0.218 & 0.938 & 0.362 & 0.781 \\ 0.446 & 0.342 & 0.388 & 0.356 & 0.298 & 0.411 \end{pmatrix}$$

GRAFICO DE TENSIONES

i := 1 .. 5

y_i :=

x_i :=

ϕ_i :=

−1.502	−0.482
−0.5335	−0.241
−0.255	0
0.533	0.5
0.94	1.0

0
0.258
0.375
0.335
0

$$\frac{1606 + 1631 + 1387 + 1384}{4} = 1502$$

$$\frac{947 + 937 + 938}{3} = 940.667$$

$$\frac{696 + 371}{2} = 533.5$$

$$\frac{303 + 292 + 382 + 196 + 218 + 388}{6} = 296.5$$

