

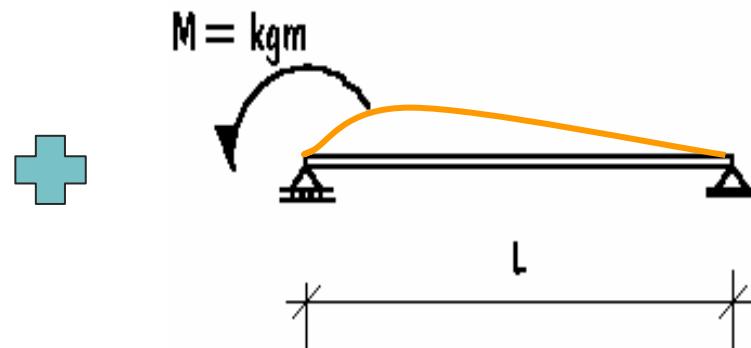
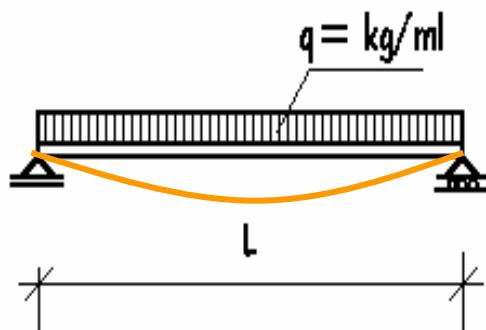
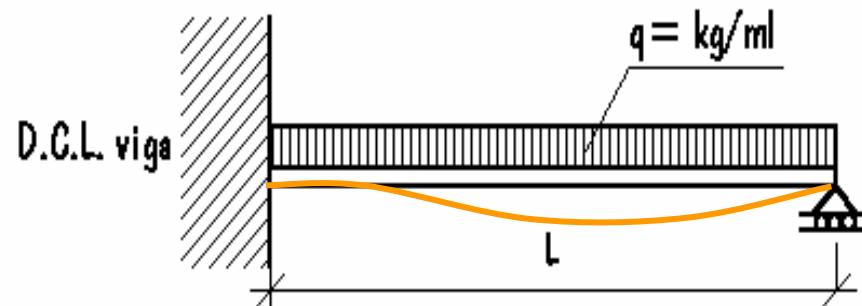
004

VIGAS HIPERESTÁTICAS

Verónica Veas B. – Gabriela Muñoz S.

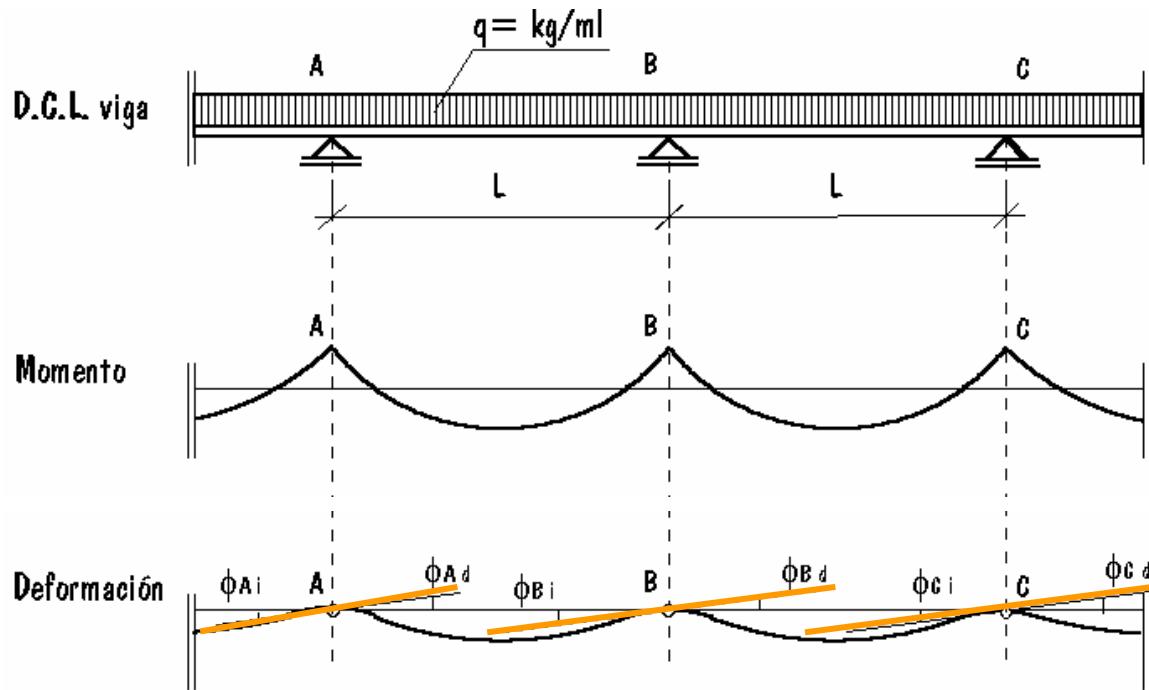


a) VIGAS HIPERESTATICAS POR EMPOTRAMIENTO



\emptyset empotramiento=0

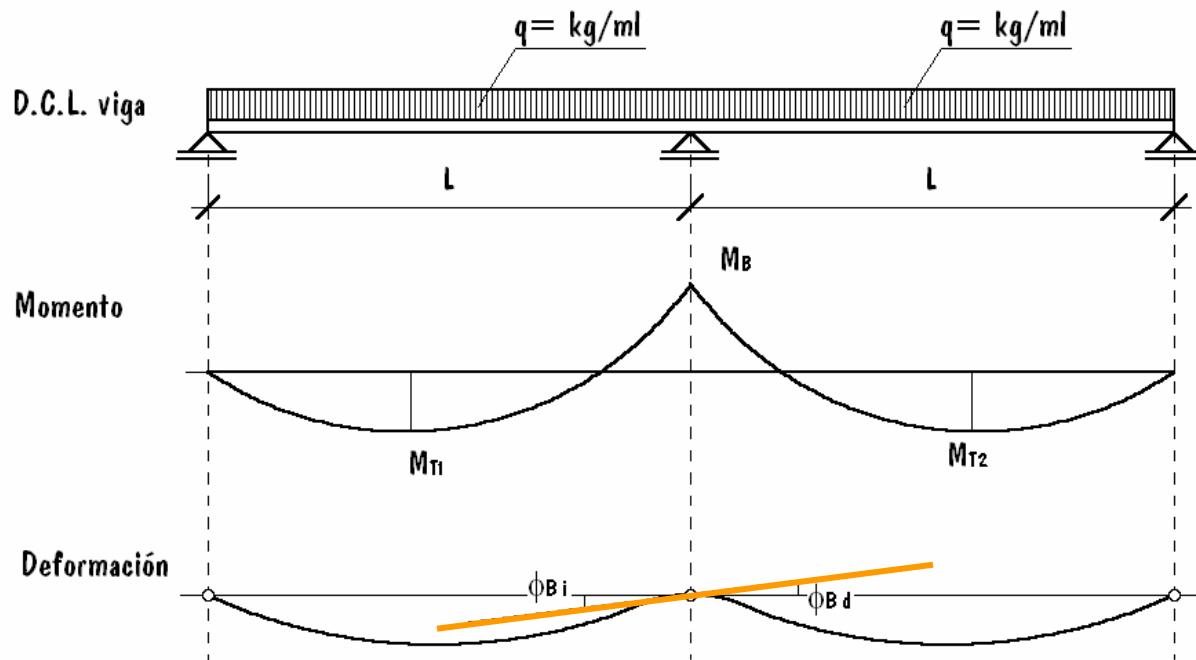
b) VIGAS HIPERESTATICAS POR CONTINUIDAD



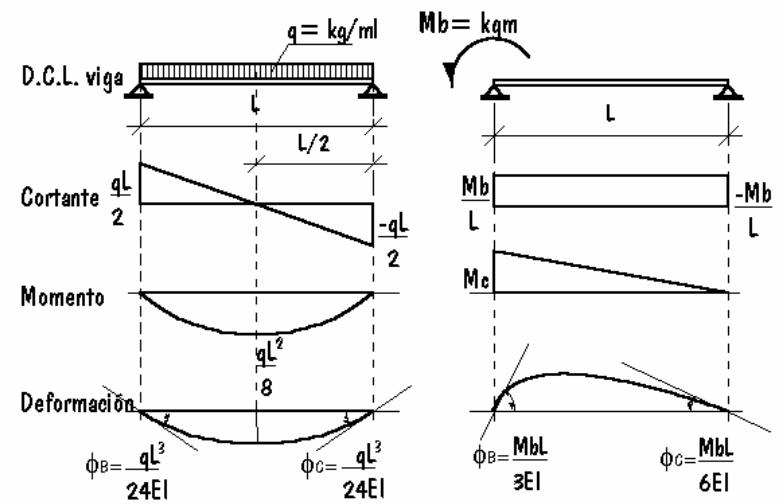
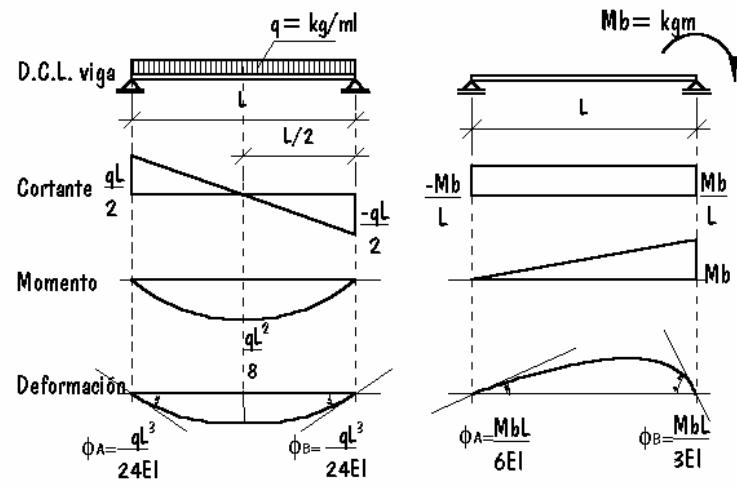
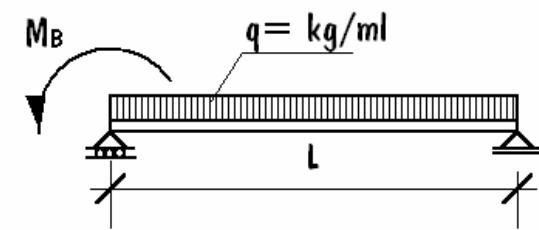
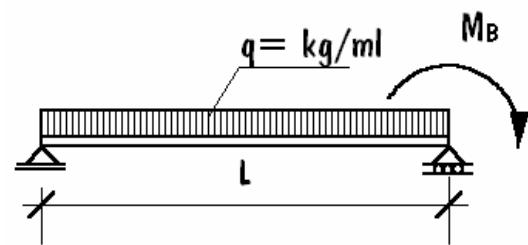
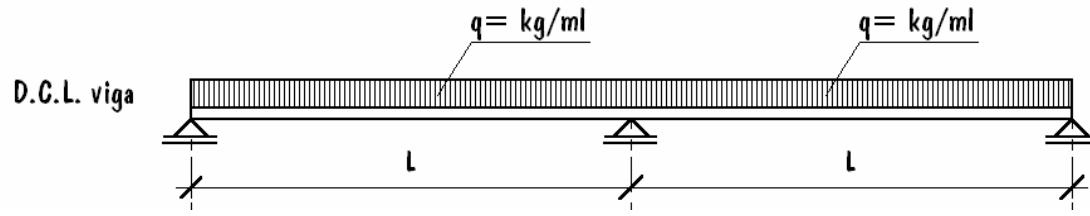
$$\phi_{B \text{ izquierdo}} = -\phi_{B \text{ derecho}}$$

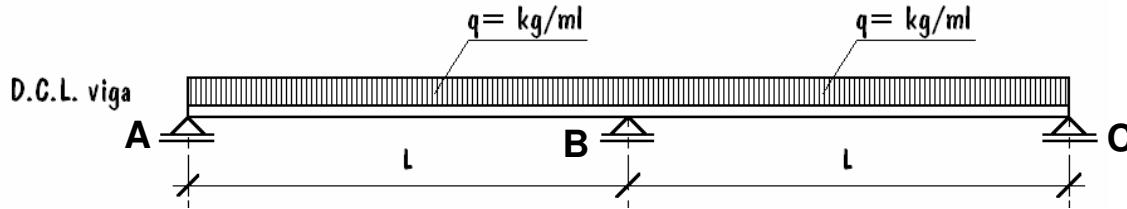
por ángulos opuestos por el vértice

VIGA DE DOS TRAMOS CON CARGA UNIFORMEMENTE REPARTIDA



$$\phi_{B_{\text{izquierdo}}} = -\phi_{B_{\text{derecho}}}$$





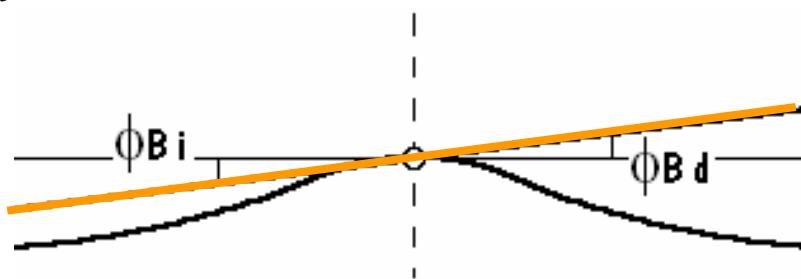
Se igualan los valores de ángulos a ambos lados del apoyo B para determinar el momento de continuidad entre ambos tramos.

$$\sum \phi_B \text{ Izquierdo} = -\sum \phi_B \text{ derecho}$$

$$-\frac{qL^3}{24EI} + \frac{M_B L}{3EI} = -\left(-\frac{qL^3}{24EI} + \frac{M_B L}{3EI}\right)$$

$$\frac{2M_B L}{3EI} = \frac{qL^3}{12EI} \quad \dots * EI/L$$

$$M_B = \frac{qL^2}{8EI}$$



$$R_B = \frac{qL}{2} + \frac{M_B}{L} = \frac{5qL}{8}$$

$$R_C = \frac{qL}{2} - \frac{M_B}{L} = \frac{3qL}{8}$$

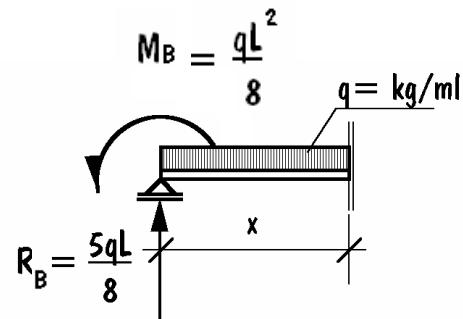
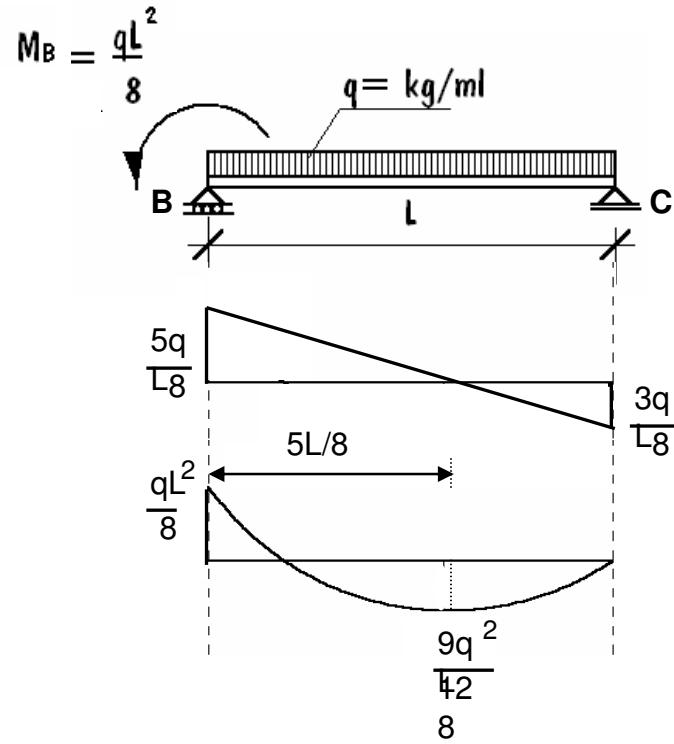
$$Mx = \frac{5qLx}{8} - \frac{qx^2}{2} - \frac{qL^2}{8}$$

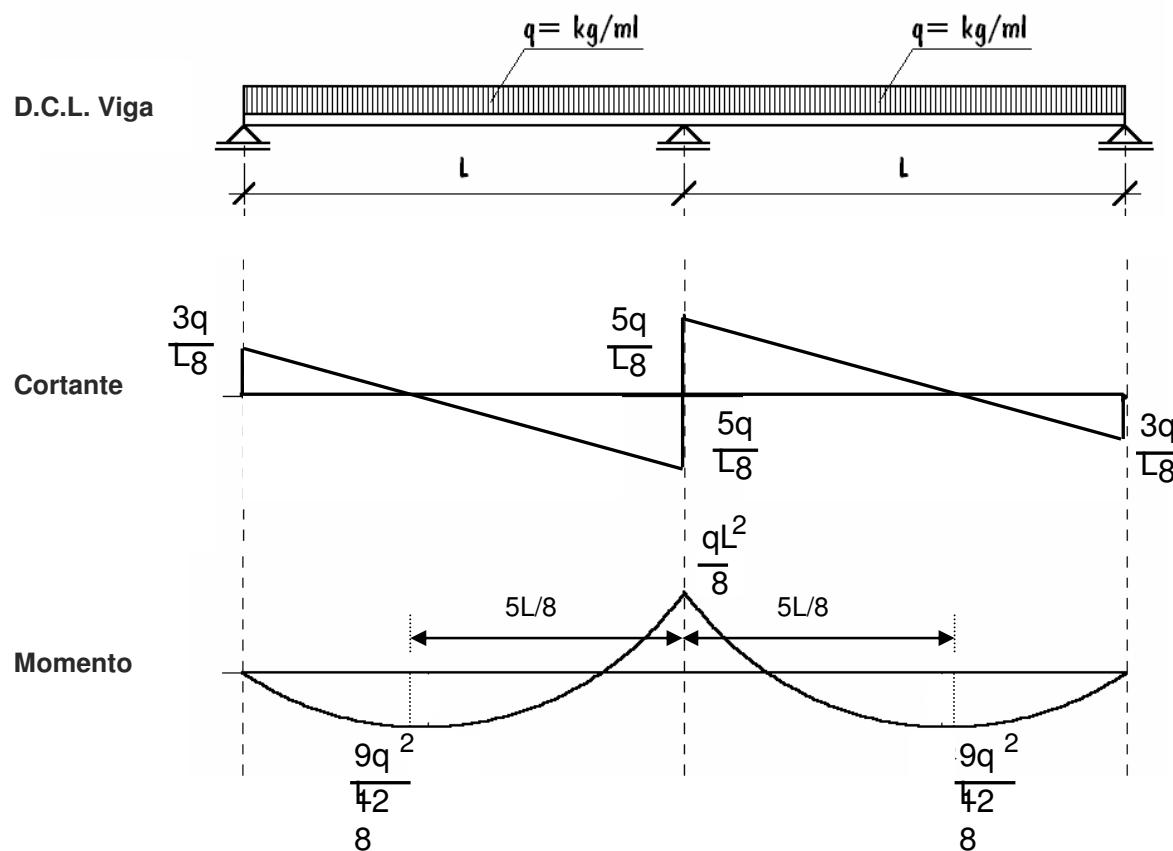
$$V_x = 0$$

$$\frac{5qL}{8} - qx = 0 \quad x = \frac{5L}{8}$$

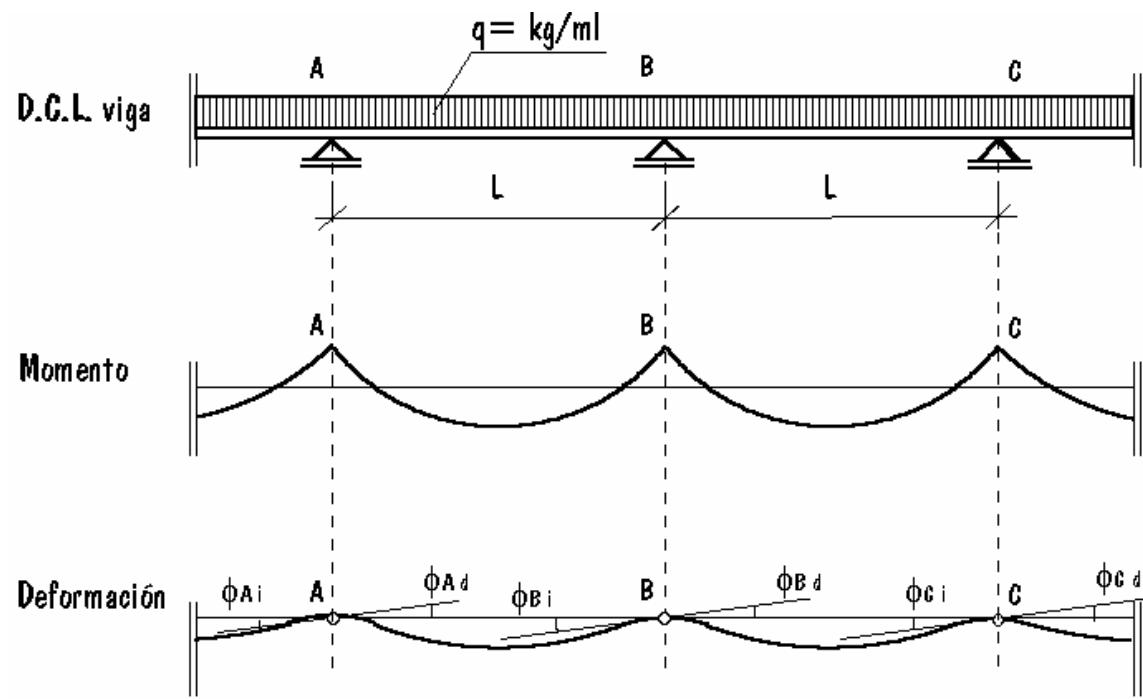
$$M_{MAX} = \frac{25qL^2}{64} - \frac{25qL^2}{128} - \frac{qL^2}{8}$$

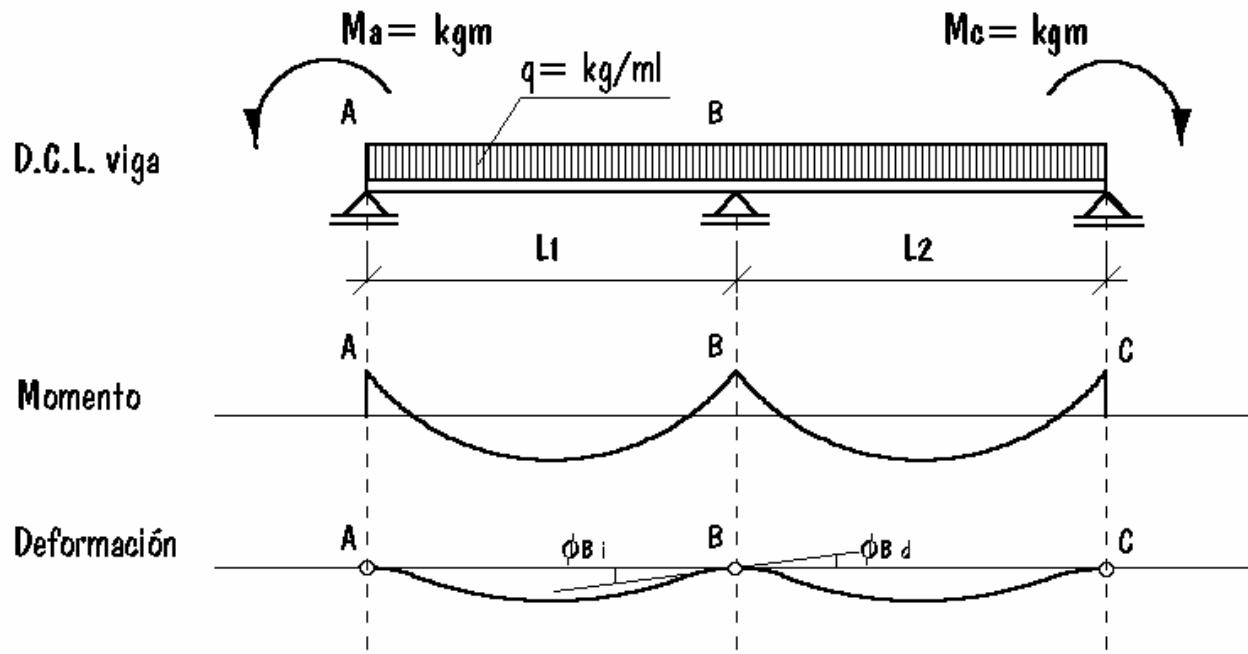
$$M_{MAX} = \frac{9qL^2}{128}$$



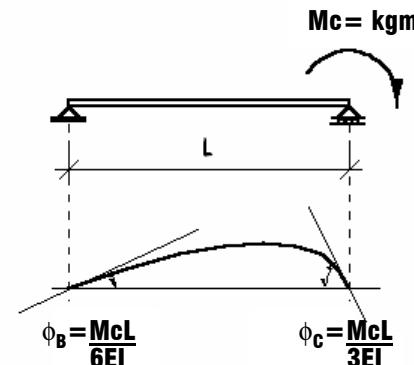
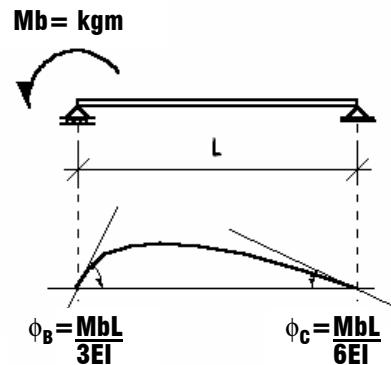
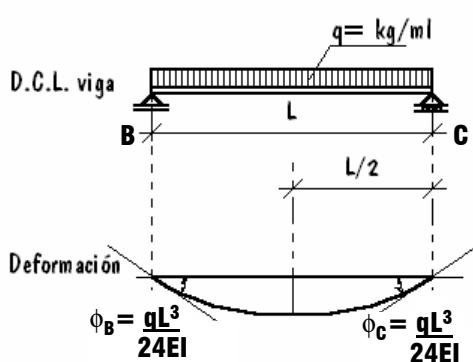
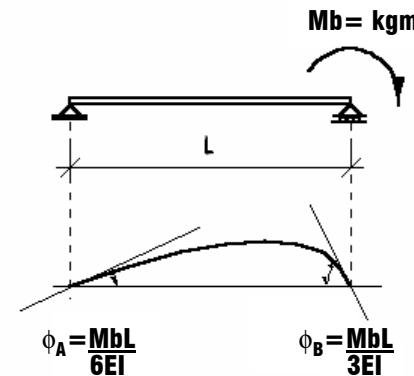
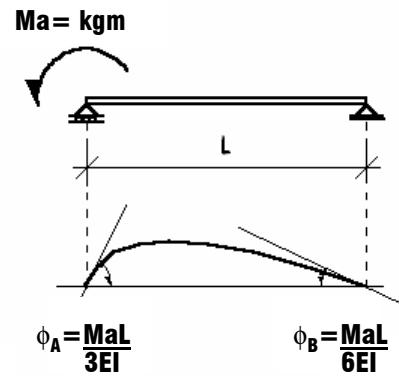
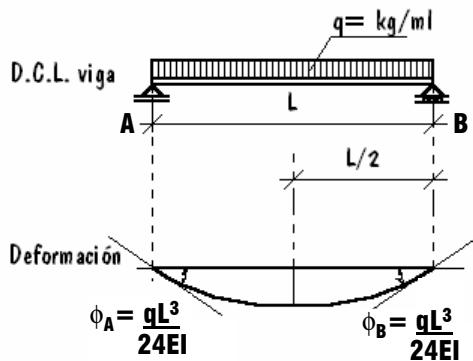


TEOREMA DE LOS TRES MOMENTOS O CLAPEYRON





$$\Sigma \phi_B \text{ izquierdo} = -\Sigma \phi_B \text{ derecho}$$



$$\Sigma \phi B_{\text{izquierdo}} = -\Sigma \phi B_{\text{derecho}}$$

$$-\frac{qL_1^3}{24EI} + \frac{MaL_1}{6EI} + \frac{MbL_1}{3EI} = -\left[\frac{qL_2^3}{24EI} + \frac{MbL_2}{3EI} + \frac{McL_2}{6EI} \right]$$

$$\frac{MaL_1}{6EI} + \frac{MbL_1}{3EI} + \frac{MbL_2}{3EI} + \frac{McL_2}{6EI} = \frac{qL_1^3}{24EI} + \frac{qL_2^3}{24EI}$$

Reemplazando L/EI por λ (módulo de flexibilidad)

$$\frac{Ma\lambda_1}{6} + \frac{Mb\lambda_1}{3} + \frac{Mb\lambda_2}{3} + \frac{Mc\lambda_2}{6} = \frac{qL_1^2\lambda_1}{24} + \frac{qL_2^2\lambda_2}{24} /*6$$

Al amplificar la expresión 6 veces se obtiene

$$Ma\lambda_1 + 2Mb\lambda_1 + 2Mb\lambda_2 + Mc\lambda_2 = 6 \left[\frac{qL_1^2\lambda_1}{24} + \frac{qL_2^2\lambda_2}{24} \right]$$

$$Ma\lambda_1 + 2Mb(\lambda_1 + \lambda_2) + Mc\lambda_2 = 6 \left[\frac{qL_1^2\lambda_1}{24} + \frac{qL_2^2\lambda_2}{24} \right]$$



Si $EI = \text{constante}$ y $\lambda = L/EI$ $\lambda = L$

Reemplazando $\lambda = L$ en la ecuación se tiene:

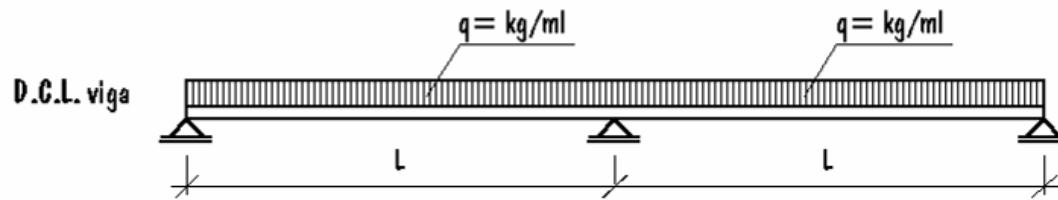
$$MaL_1 + 2Mb(L_1 + L_2) + McL_2 = 6 \left[\frac{qL_1^3}{24} + \frac{qL_2^3}{24} \right]$$

Reemplazando $\frac{qL_1^3}{24}$ por Tc_1 y $\frac{qL_2^3}{24}$ por Tc_2

$$\boxed{\mathbf{MaL_1 + 2Mb(L_1+L_2) + McL_2 = 6(Tc_1 + Tc_2)}}$$

APLICACIÓN DEL TEOREMA DE CLAPEYRON

VIGA DE DOS TRAMOS CON CARGA UNIFORMEMENTE REPARTIDA



$$MaL_1 + 2Mb(L_1+L_2) + McL_2 = 6(Tc_1 + Tc_2)$$

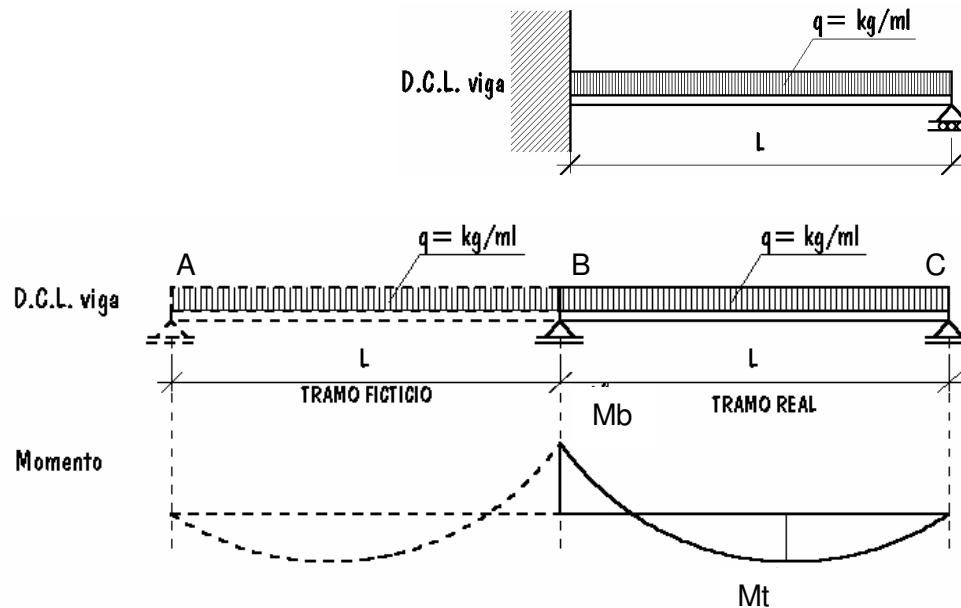
$$0L_1 + 2Mb(L_1+L_2) + 0L_2 = 6 \left[\frac{qL_1^3}{24} + \frac{qL_2^3}{24} \right]$$

$$2Mb(L_1+L_2) = \frac{qL_1^3}{4} + \frac{qL_2^3}{4} \quad \text{Si } L_1=L_2$$

$$2Mb 2L = \frac{qL^3}{2}$$

$$Mb = \frac{qL^2}{8}$$

VIGA EMPOTRADA EN UN EXTREMO Y APOYADA EN EL OTRO CON CARGA UNIFORMEMENTE REPARTIDA



$$M_a L_1 + 2M_b (L_1 + L_2) + M_c L_2 = 6 (T_{c1} + T_{c2})$$

$$00 + 2M_b (0+L) + 0L = 6 \left[0 + \frac{qL^3}{24} \right]$$

$$2M_b L = \frac{qL^3}{4}$$

$$M_b = \frac{qL^2}{8}$$